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MODELING OF DISPERSION EFFECT FOR INTERMITTENT FLOW IN PREMISE PLUMBING SYSTEMS

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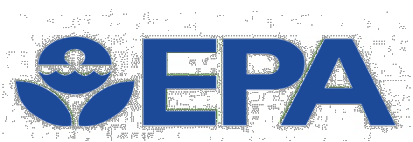
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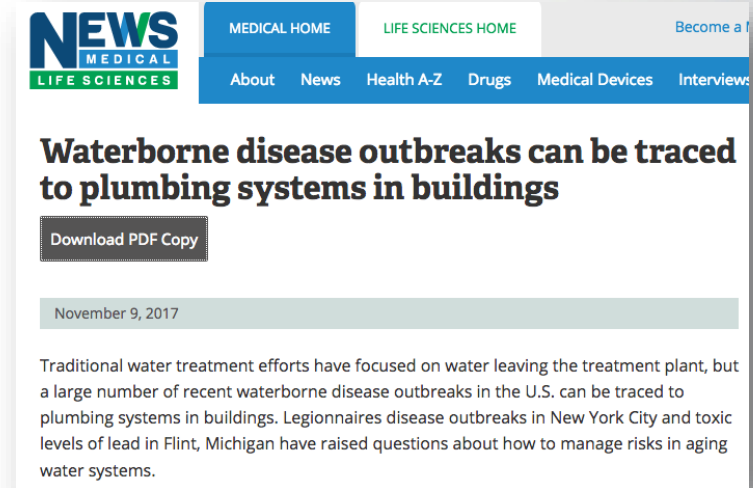
Outline

- Introduction
- Dispersion Modeling
- Literature Reviews
- Methods
- Results
- Conclusions

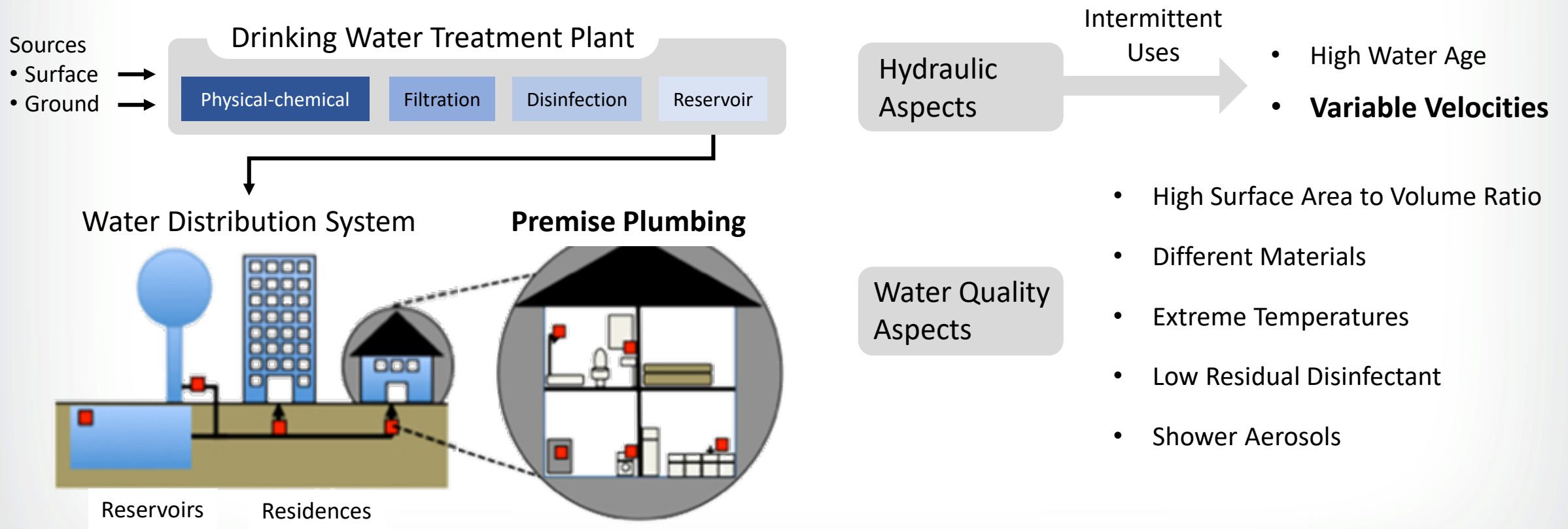


Introduction

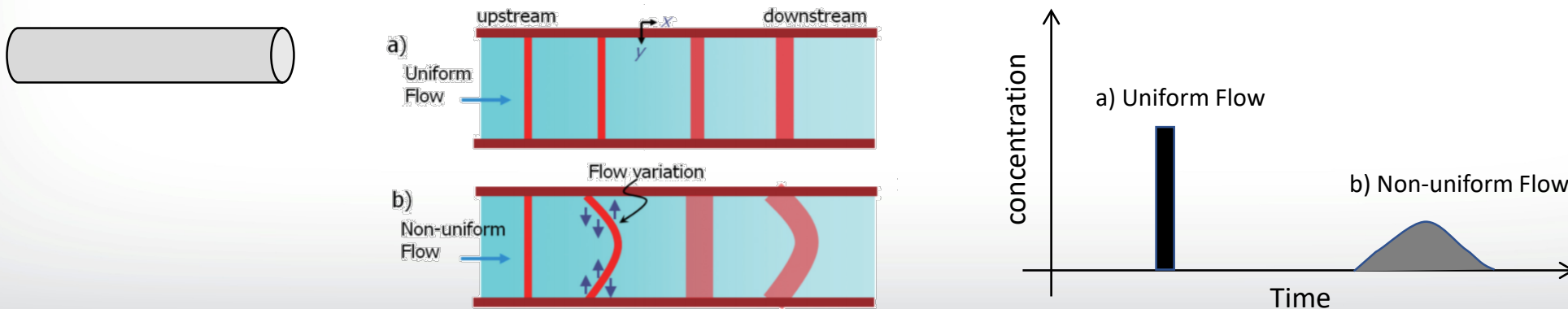
- Water quality in premise plumbing system (PPS)
 - Raised public awareness of importance of safe drinking water in homes and buildings
 - Risk of exposure to contaminants from water in homes or buildings
- Quality of water at the end use is affected by numerous factors
 - plumbing materials, size, water chemistry, water use
- Concentrations of contaminants in a building can be changed due to hydraulic changes



- Premise plumbing has several unique characteristics



- EPANET does not accurately simulate PPS
 - EPANET solves advection and reaction equations.
 - EPANET assumes uniform flow in the pipe due to the dominant turbulent flow in advective transport.
- Dispersion plays an important role in the simulations
 - Dead end, laminar flow, transient flow, dispersion coefficient, chlorine decay
- Modeling of PPS also needs to consider dispersion due to the change of velocity in the pipe, specially in the laminar flow





Literature Reviews

Taylor, Aris

Dispersion equations for laminar and turbulent flow

1953 - 54

Axworthy and Karney

Low velocity/high dispersion flow - Dispersion plays an important role in laminar flow in the pipe flow

1996

Lee and Buchberger

Dispersion equations for unsteady laminar flows

2004

Abokifa et al.

Extended ADRNET to consider spatial demand distribution - WUDESIM

2016

1979

Fischer et al.

A moment method to estimate the dispersion coefficient based on the concentration time profiles in the rivers

2001

Tzatchkov et al.

Advection-dispersion transport is more close to actual water quality for intermittent flow in water distribution networks

2006

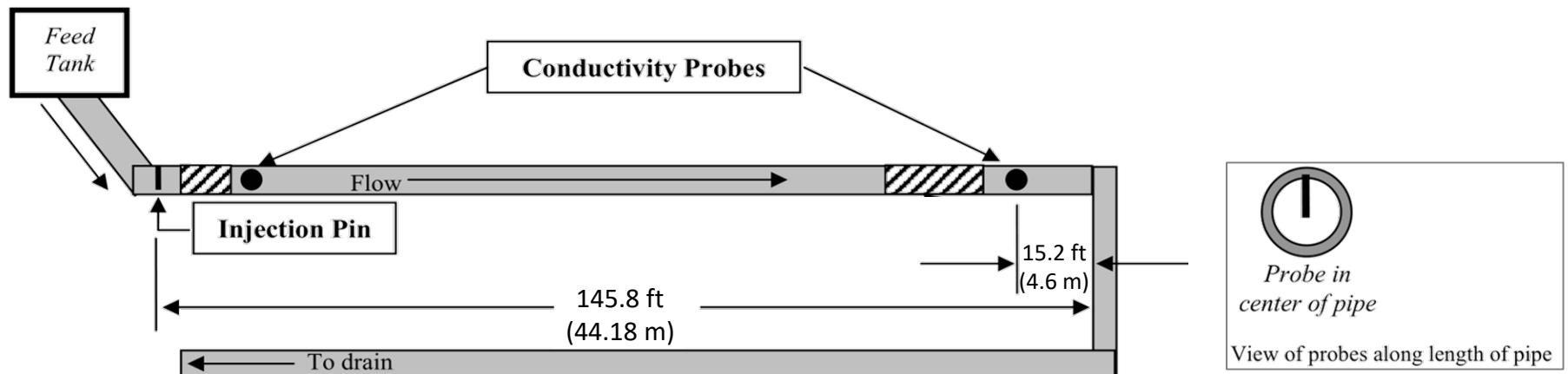
Li and Buchberger

An attempt to combine PRPmodel with 1D ADR together - ADRNET

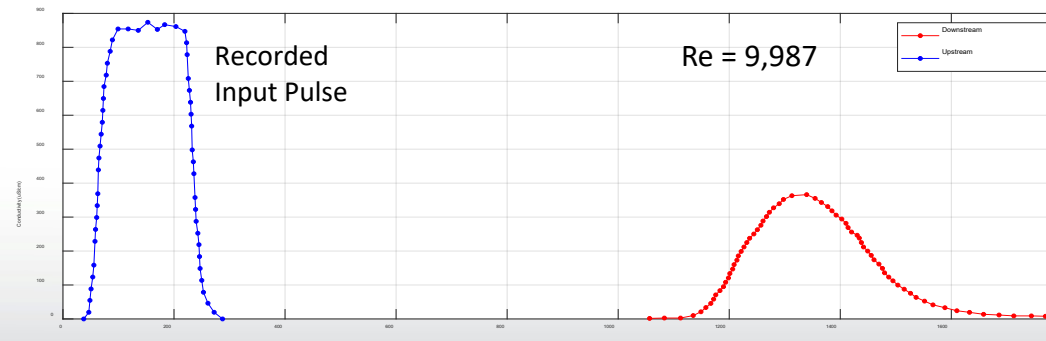
Most research was based upon *Taylor's Dispersion Equation!*

Tracer Study

- Experimental setup*
- Tracer injection study at US EPA T&E



- An example of measurements - conductivity versus time





Estimation of Dispersion Coefficients

- Dispersion coefficients are estimated using different methods

- Taylor Equation

$$D = \begin{cases} \frac{a^2 u^2}{48 D_m} & Re < 2,300 \quad \text{Laminar dispersion} \\ 10.1 a u_* & 4,000 < Re \quad \text{Turbulent dispersion} \end{cases}$$

- Method of Moments

$$D = \frac{1}{2} \frac{d\sigma^2}{dt} \approx \frac{1}{2} \frac{\Delta\sigma^2}{\Delta t}$$

- Heuristic Method

- Finding dispersion coefficient heuristically in the analytical equation
 - Parameters in the analytical equation (C_o, t_o, D)

$$C(x, t) = \begin{cases} C_o A(x, t) & 0 < t \leq t_o \\ C_o (A(x, t) - A(x, t - t_o)) & t > t_o \end{cases}$$

$$A(x, t) = \frac{1}{2} \operatorname{erfc} \left[\frac{x - ut}{\sqrt{4Dt}} \right] + \sqrt{\frac{u^2 t}{\pi D}} \exp \left[-\frac{(x - ut)^2}{4Dt} \right] - \frac{1}{2} \left(1 + \frac{ux}{D} + \frac{u^2 t}{D} \right) \exp \left(\frac{ux}{D} \right) \operatorname{erfc} \left[\frac{x + ut}{\sqrt{4Dt}} \right]$$



Estimation of Dispersion Coefficients

- Parameters in the analytical equation (C_o, t_o, D)

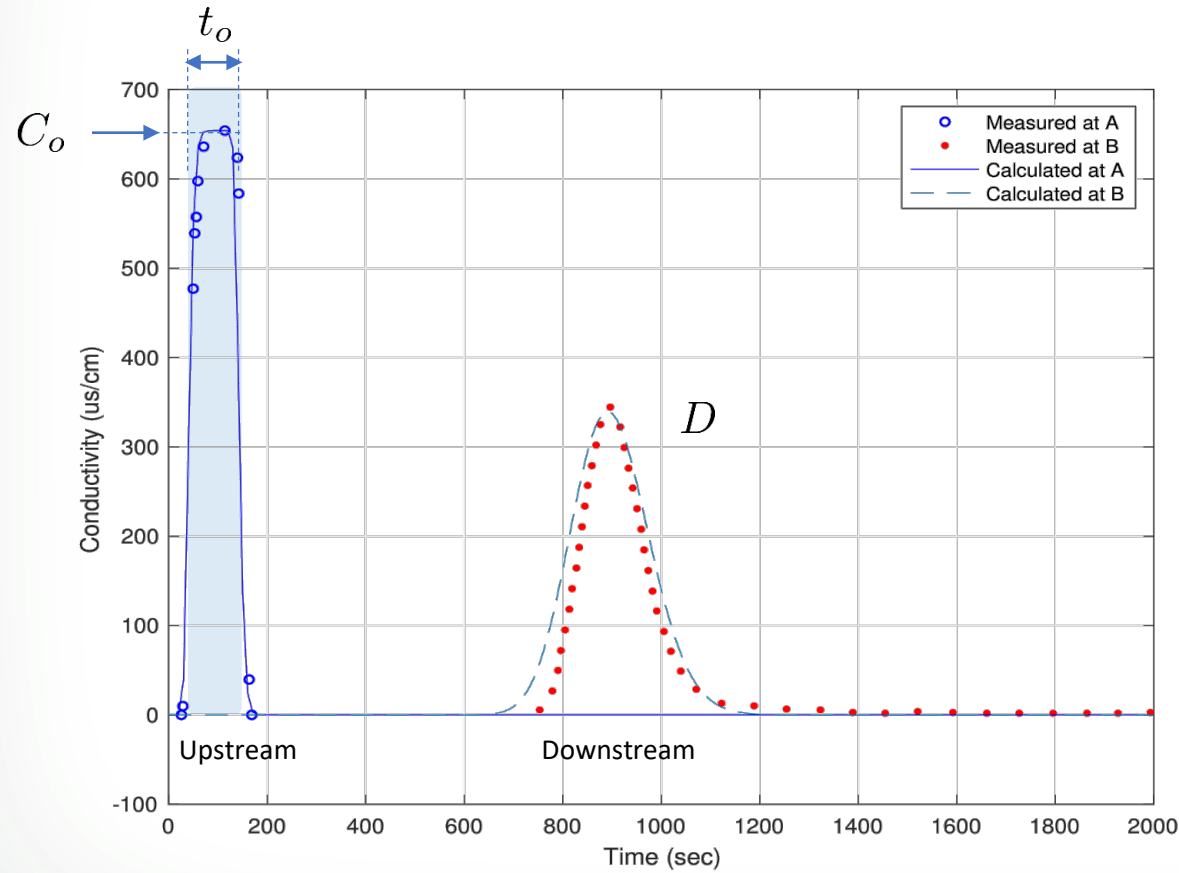


Figure 1. An example of tracer movement. The observed data was expressed with the dotted points and analytical solution was shown in continuous line ($Re = 4,960$)

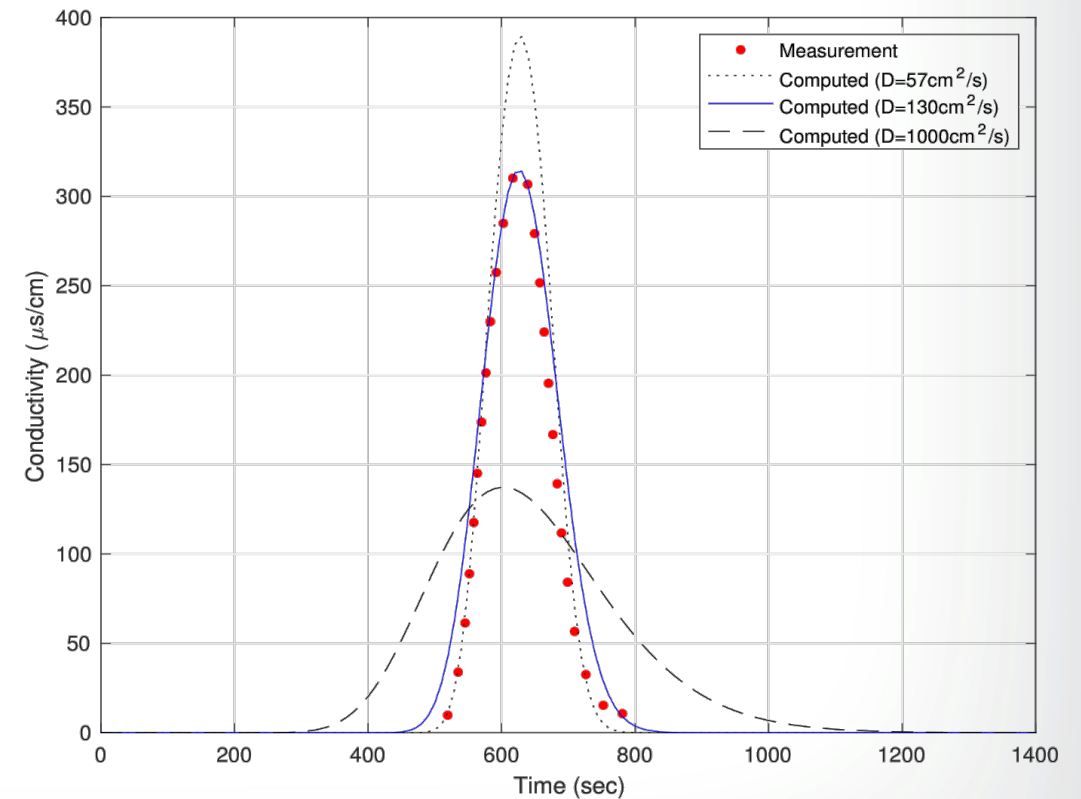
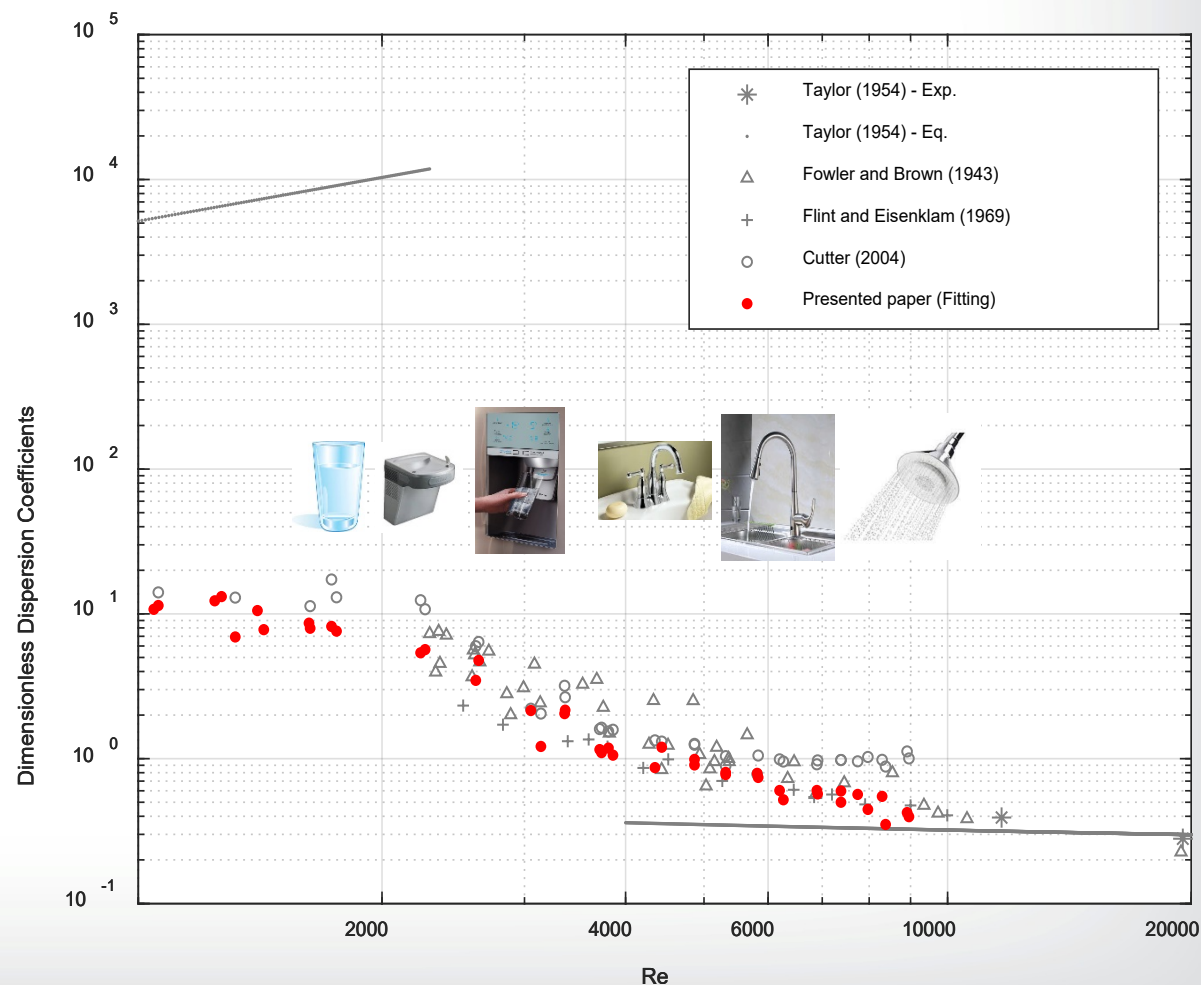


Figure 2. Concentration profiles with different dispersion coefficients and measurement data (plotted with red points)

- Estimated dimensionless dispersion coefficients
 - Comparison with literatures
 - Taylor dispersion does not agree with experimental data for $Re < 10,000$
 - For a home plumbing system
 - Maximum water usages*
 - Faucet (kitchen): 2.2 GPM
 - Faucet (bathroom): 0.5 – 1.5 GPM
 - Toilet : 1.6 – 3.6 GPM
 - Shower: 2 – 2.5 GPM
 - Calculated Reynolds number for a pipe (internal diameter of 3/4 inches)
 - 2.21 GPM – $Re = 10,000$
 - 1.55 GPM – $Re = 7,000$

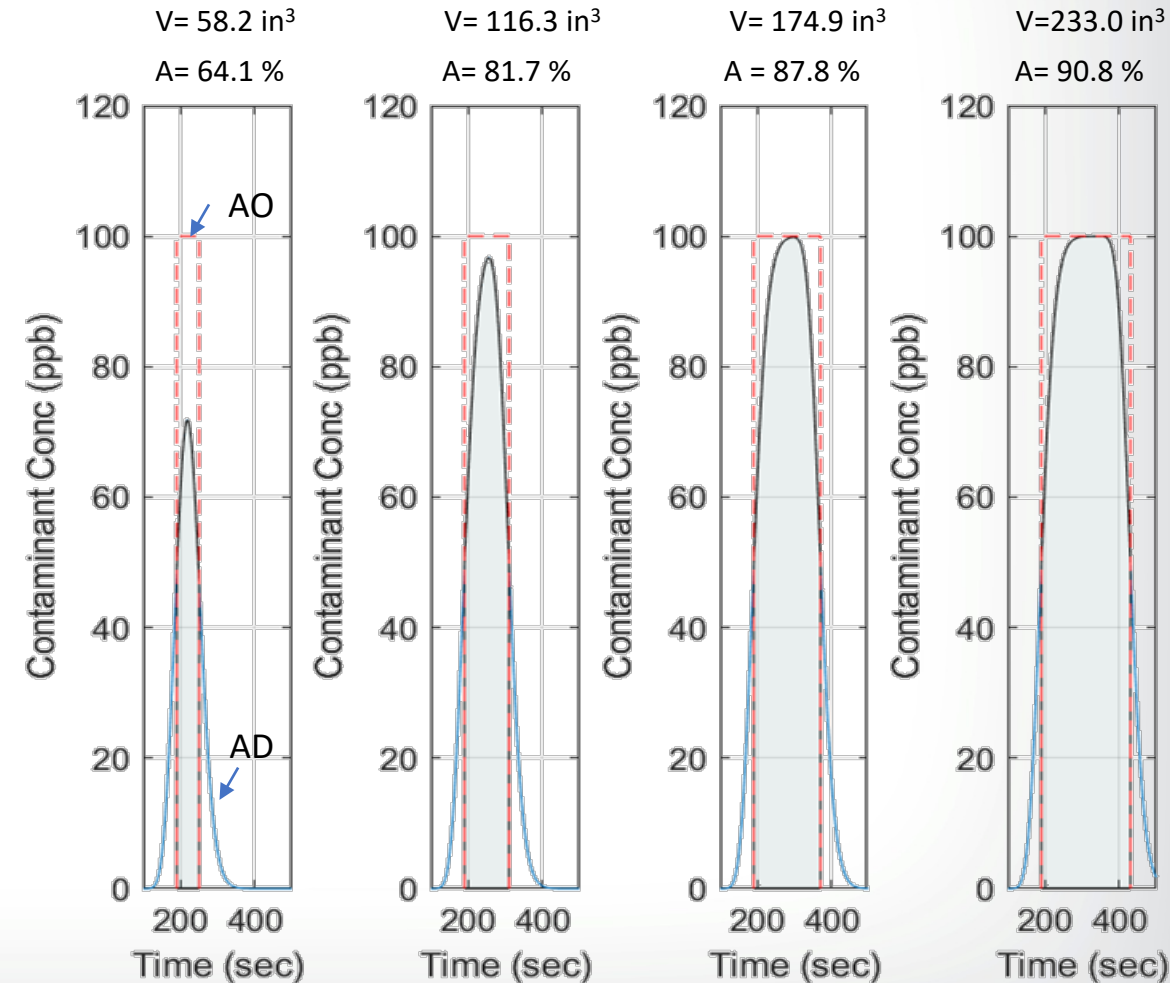




Results

- Dispersion effects to advective transport
 - Effects of various volumes of contaminant to advective transport
 - Comparison of percentage agreement between advection only (EPANET) and advection-dispersion equation
 - Compared the area under the curves between advection only and advection dispersion - converted to percentage
 - Advection only (AO) is shown as dashed lines and advection-dispersion (AD) is shown as solid lines

Re = 1,332, Diameter = 5/8 inches, D = 20.6 in²/s

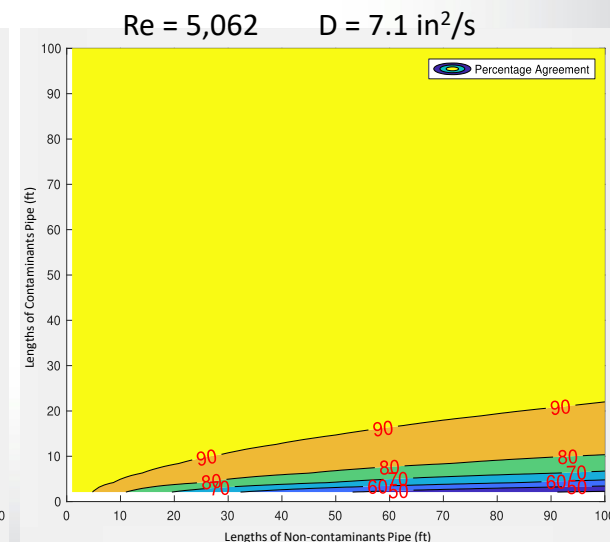
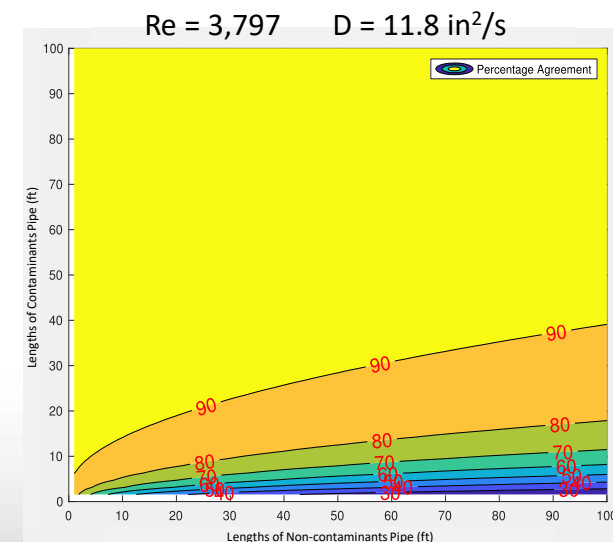
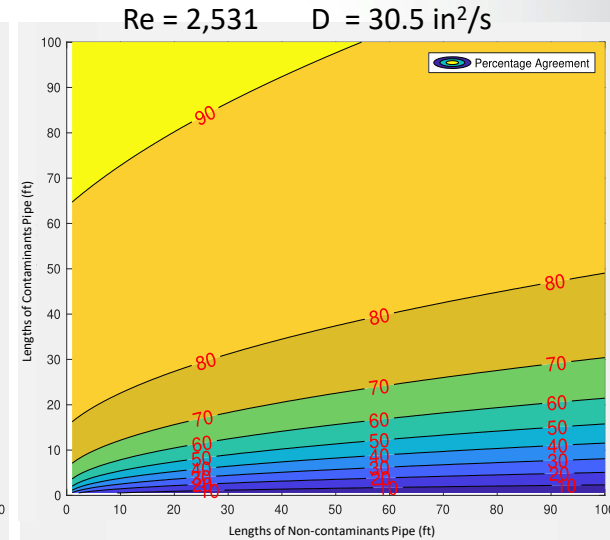
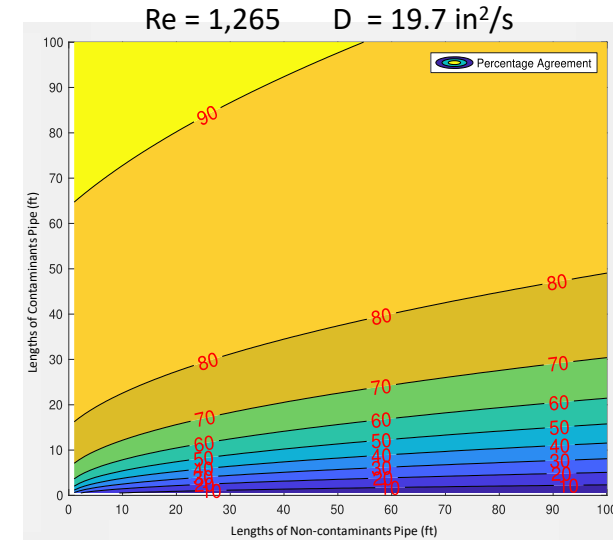


V: Contaminant volume, A: Area ratio under rectangular, D: Dispersion coefficient



Results

- Dispersion effects to advective transport
 - Changing velocity and various volumes of contaminant
 - Contour lines are the percentage agreement between AO and AD
 - Velocity increases, the higher numbers of percentage agreement are shown
 - When the volumes of contaminant increases, the percentage of agreement increases
 - Advection only equation
 - valid for the turbulent region
 - Small volume of contaminant
 - the advection only method may not be accurate due to the dispersion





Conclusion

- Hydraulic modeling of a PPS needs to consider dispersion effects
- Taylor dispersion is not applicable to practical application of premise plumbing system
 - Shower, kitchen, bathroom, refrigerator, drink a cup of water, and etc.
 - Only valid for fully developed turbulent region ($Re > 10,000$)
- Dimensionless dispersion coefficients:
 - For the pipe flow of transition and turbulent ($2,000 < Re < 10,000$)
 - Dimensionless dispersion coefficient varies between 0.3 and around 10.
 - For the pipe flow of laminar ($1,000 < Re < 2,000$)
 - Dimensionless dispersion coefficient seems to be around 10.
- Dispersion effects to advective transport in a PPS were investigated by changing velocity and various volumes of contaminant



Thank you!

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