Statistical comparison of performance reference compound (PRC)-based methods for calculating C_{free}



BACKGROUND

- Ideally, during a passive sampling deployment all target contaminants achieve equilibrium with the passive sampler:
 - Freely dissolved concentration (C_{free}) can be calculated: $C_{free} = \frac{C_{Passive Sampler}}{\nu}$ K_{Passive} Sampler–Water
 - C_{Passive Sampler} = concentration measured in passive sampler K_{Passive Sampler-Water} = partition coefficient relating polymer and water concentrations
- In reality, during a passive sampling deployment many target contaminants do not achieve equilibrium with the passive sampler
 - Under in situ conditions & for larger, high octanol-water (K_{OW}) target contaminants
- If Equation 1 is used, results in under-estimating C_{free}
 - Under-estimating exposure and risk

USE OF PRCS

- Performance Reference Compounds (PRCs) are an increasingly common tool for calculating adjustment factors for non-equilibrium conditions
 - For example, the fractional equilibrium (f_{eq})
- Using PRCs and feq, the freely dissolved concentration (C_{free}) can be calculated: Passive Sampler* $\frac{1}{feq}$ [2] $C_{free} =$

under non-equilibrium conditions

*K*_{Passive} Sampler–water

- Currently, several models available for using PRC data to calculate feet
- This variety of models creates confusion for users as to which one(s) to apply Users = risk assessors & remedial project managers at contaminated sites Not necessarily passive sampling experts

OBJECTIVES

- Generate a large passive sampler dataset and statistically compare the calculation of C_{free} using four common PRC models
 - Use C_{free} as the dependent variable
 - Examine effect of polymer thickness on 'rate' of achieving equilibrium
 - Hypotheses:
 - For a given contaminant:

 $H_0: C_{free}^{Model1} = C_{free}^{Model2} = C_{free}^{Model3} = C_{free}^{Model4}$ $H_1: C_{free}^{Model1} \neq C_{free}^{Model2} \neq C_{free}^{Model3} \neq C_{free}^{Model4}$

Recommend a model(s) for passive sampler users to apply

¹US EPA, ORD/NHEERL, AED, Narragansett, RI, USA, burgess.robert@epa.gov ²Duke University, Durham, North Carolina USA, abigail.joyce@duke.edu

MATERIALS AND METHODS

- Deployed (30 days) low density polyethylene (PE) samplers at three water column stations in the PCB-contaminated New Bedford Harbor Superfund site (MA, USA) (Figure 1):
- Three thicknesses: 12, 51 and 76 μm
- Located samplers one meter above bottom in the water column (Figure 2)
- 9 sets of possible comparisons here we will focus on NBH2
- Target contaminants were 27 PCB congeners
- Six ¹³C-labelled PCB PRCs: 8, 28, 52,101,138 and 180
- Triplicate replication per station: ANOVA with Fisher's Test used to detect differences



Figure 1: Sampling stations in New Bedford Harbor Superfund site (MA, USA)



Figure 2: Passive sampler deployment configuration

 $C_{free}^{\infty} = C_{free}^t$

- Four models compared (citation below):
 - (1) Equilibrium assumed: Target contaminants assumed to achieved equilibrium
 - (2) First order model: PRC data fit to simple first order kinetics model to estimate fractional equilibrium (f_{ea}) $C_{free}^{\infty} = \frac{C_{PS}}{K_{PS}} * (1 - e^{-k_e t})$ (Adams et al. 2007)
 - (3) Exchange rate-based model: First order model applies PRC data to calculate corrected exchange rates (R_s) with a nonlinear least squares (NLS) fit (Booij and Smedes 2010)
 - $C_{free}^{\infty} = \frac{C_{PS} * m_p}{R_s * t}$

 $\frac{\delta C_{PS}}{\delta t} = D_{PS} \frac{\delta^2 C_{PS}}{\delta x^2}$

(4) Diffusion-based model: Rate of PRC diffusion through polymer and water used to determine magnitude of f_{eq} $\frac{\boldsymbol{\delta}C_{DBL}}{\boldsymbol{\delta}t} = D_W \frac{\boldsymbol{\delta}^2 C_{DBL}}{\boldsymbol{\delta}x^2}$

(Fernandez et al. 2009, Thompson et al. 2015)

Adams RG, R Lohmann, LA Fernandez, JK MacFarlane, PM Gschwend. Polyethylene Devices: Passive Samplers for Measuring Dissolved Hydrophobic Organic Compounds in Aquatic Environments. *Environmental Science and Technology* **2007**, *41*: 1317–1323.

Booij K, F Smedes. An Improved Method for Estimating in Situ Sampling Rates of Nonpolar Passive Samplers. Environmental Science & Technology 2010, 44: 6789-6794.

Fernandez LA, CF Harvey, PM Gschwend. Using Performance Reference Compounds in Polyethylene Passive Samplers to Deduce Sediment Porewater Concentrations for Numerous Target Chemicals. Environmental Science & Technology 2009, 43: 8888-8894.

Thompson JM, CH Hsieh, RG Luthy. Modeling Uptake of Hydrophobic Organic Contaminants into Polyethylene Passive Samplers. *Environmental Science & Technology* **2015**, *49:* 2270– 2277

Robert M. Burgess¹ and Abigail S Joyce²



- \bullet In most cases, the sampling rate and diffusion models resulted in statistically-identical C_{free}s
- ◆ More validation of modelled C_{free} values is needed
- Models available in spreadsheet and graphic user interfaces (GUI)
- Diffusion model GUIs available on-line (e.g., U.S. EPA & SERDP websites)



• Available comparable data suggests diffusion and sampling rate models provide accurate estimates of C_{free}

Recommend use of diffusion and sampling rate models for analyzing PRC data to calculate C_{free}