

Estimation of Air-Toxic Emissions from Highway Vehicles
in the Motor Vehicle Emissions Simulator (MOVES 2014)

DRAFT REPORT

USEPA Office of Transportation and Air Quality
Assessment and Standards Division

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1 Background

This document describes the data and methods used to estimate emissions of toxic compounds emitted from for highway vehicles in the MOVES2014 database and model. The current release of the MOVES database (MOVES2014) includes substantial updates to inputs and structures used to estimate toxic emissions, incorporating data from recent programs conducted on recently manufactured vehicles employing current technologies. It also includes the capability to estimate emissions for ethanol blends containing more than 10% ethanol, including E15, E20, E70, and E85 (71-100% ethanol).

For light-duty vehicles manufactured prior to 2001, exhaust emissions for several compounds (including benzene, 1,3-butadiene, acetaldehyde and formaldehyde), are estimated using algorithms developed for the Complex Model for Reformulated Gasoline, developed in the early 1990's for the Federal Reformulated Gasoline Rule.¹ These algorithms are used to calculate toxic to volatile organic compound (VOC) ratios based on fuel composition, and the ratios are then applied to VOC mass. For vehicles manufactured in 2004 and later, emissions of selected toxics are estimated through calculations based on models developed using data generated by EPA's program. These algorithms were developed to provide the capability to account for changes in toxic emissions attributable to changes in fuel properties, as specified by users.

Compounds emitted as constituents of exhaust but not included in the Complex or EPA's models were estimated using simpler approaches that do not explicitly account for changes in fuel properties.

For emissions through evaporative processes, simpler approaches were used. In some cases, these approaches account for two fuel properties, but typically do not account for fuel properties.

1.1 Air Toxics

Through MOVES, users can estimate inventories for all compounds emitted from highway vehicles that are also identified as air toxics in the National Emission Inventory (NEI) and National Air Toxics Assessment (NATA), and for which there are adequate data to develop emission estimates. This list of pollutants is provided in Table 1.1. These pollutants are organized into four categories:

- 1) Gaseous hydrocarbons
- 2) Polycyclic aromatic hydrocarbons (PAHs): This class is defined as hydrocarbons containing fused aromatic rings. These compounds can be found in the gaseous phase, particulate phase, or both, depending on properties of the compound, particle characteristics and atmospheric conditions
- 3) Dioxins and furans – polychlorinated organic compounds which are persistent and bioaccumulative

4) Metals

The pollutant “xylenes” represents the sum of emissions from three isomers of xylene: o-xylene, m-xylene, and p-xylene. MOVES also reports three forms of mercury: elemental gaseous, divalent gaseous (a reactive form) and particulate phase. Moreover, arsenic is reported as the total mass of all organic and inorganic arsenic compounds. However, emissions data for mobile sources all come from measurements of elemental arsenic mass.

Table 1. Gaseous Hydrocarbons included in MOVES2014.

Pollutant	pollutantID	CAS Number
1,3-Butadiene	24	106990
2,2,4-Trimethylpentane	40	540841
n-Hexane	55	110543
Acetaldehyde	26	75070
Formaldehyde	25	50-00-0
Propionaldehyde	58	123386
Acrolein	27	107028
Methyl-Tertiary-Butyl Ether (MTBE)	22	1634044
Ethanol	21	64175
Ethyl Benzene	52	100414
Styrene	60	100425
Benzene	20	71-43-2
Toluene	61	108883
Xylenes	62	1330207

Table 2. Polycyclic Aromatic Hydrocarbons included in MOVES2014.

Pollutant	pollutantID	CAS Number
Acenaphthene	41	83329
Acenaphthylene	42	208968
Anthracene	44	120127
Benz(a)anthracene	45	56553
Benzo(a)pyrene	46	50328
Benzo(b)fluoranthene	47	205992
Benzo(g,h,i)perylene	48	191242
Benzo(k)fluoranthene	49	207089
Chrysene	50	218019
Dibenzo(a,h)anthracene	51	53703
Fluoranthene	53	206440
Fluorene	54	86737
Indeno(1,2,3,c,d)pyrene	56	193395
Naphthalene	23	91203
Phenanthrene	57	85018
Pyrene	59	129000

Table 3. Dioxins and Furans included in MOVES2014

Pollutant	pollutantID	CAS Number
2,3,7,8-Tetrachlorodibenzo-p-Dioxin	301	17466016
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	302	40321764
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	303	39227286
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	304	57653857
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	305	19408743
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	306	35822469
Octachlorodibenzo-p-dioxin	307	3268879
2,3,7,8-Tetrachlorodibenzofuran	308	51207319
1,2,3,4,6,7,8-Heptachlorodibenzofuran	309	67562394
1,2,3,4,7,8,9-Heptachlorodibenzofuran	310	55673897
1,2,3,4,7,8-Hexachlorodibenzofuran	311	70648269
1,2,3,6,7,8-Hexachlorodibenzofuran	312	57117449
1,2,3,7,8,9-Hexachlorodibenzofuran	313	72918219
1,2,3,7,8-Pentachlorodibenzofuran	314	57117416
2,3,4,6,7,8-Hexachlorodibenzofuran	315	60851345
2,3,4,7,8-Pentachlorodibenzofuran	316	57117314
Octachlorodibenzofuran	317	39001020

Table 4. Metals included in MOVES2014.

Pollutant	pollutantID	CAS Number
Mercury (elemental gaseous)	201	200
Mercury (divalent gaseous)	202	201
Mercury (particulate)	203	202
Arsenic compounds	204	93
Chromium (Cr3+)	205	16065831
Chromium (Cr6+)	206	18540299
Manganese	207	7439965
Nickel	208	7440020

Toxics inputs for MOVES are not explicitly designed to vary by temperature. However, emissions estimated for the various hydrocarbon species do vary by temperature implicitly in that they are estimated in relation to inventories for VOC, or organic carbon (OC2.5) which are in turn estimated from total hydrocarbons (THC), which is adjusted by temperature for the start emissions process. However, for the running emissions process, THC emissions are not adjusted for temperature, and therefore most toxic emissions are also not temperature dependent, either implicitly or explicitly.

As metals are estimated directly through emission rates, these rates are assumed to be independent of operating mode and temperature. Data to account for impacts of these parameters are inadequate to model these effects in MOVES.

For 2004 and later vehicles, toxic to PM ratios differ for start versus running emissions for benzene, 1,3-butadiene, formaldehyde, acetaldehyde, acrolein and ethanol.

During model runs, emissions of toxic compounds, except for metals and dioxins/furans, are estimated as fractions of the emissions of volatile organic compounds (VOC), or in some cases organic carbon (OC_{2.5}). Metals and dioxins/furans are estimated using distance-specific emission rates. Emissions of VOC are themselves calculated from emissions of total hydrocarbons (THC). The available data and methods used to estimate toxic fractions vary for different groups of compounds. For some compounds, the toxic emissions are estimated using “complex” fractions, meaning that the fraction varies with levels of other fuel properties, such as ethanol, aromatics or RVP. For other sets of compounds, “simple” fractions are used, meaning that the fractions are constants and do not vary with other fuel properties. Note that the generalizations made here apply to evaporative as well as to exhaust emissions.

2 Exhaust Emissions

2.1 Light-Duty Vehicles (gasoline-powered): Model Year 2000 and Earlier

2.1.1 Gaseous Hydrocarbons

2.1.1.1 Vehicles operating on Fuel blends containing 0-20% Ethanol

For three sets of compounds, Table 5 summarizes the methods used to estimate toxic fractions. The specific data and methods used for each are described in further detail below.

Table 5. Calculation Methods for Gaseous hydrocarbons

Compound	Fraction Type	Basis for Estimation
Benzene	complex	Complex Model
1,3-Butadiene	complex	Complex Model
Acetaldehyde	complex	Complex Model
Formaldehyde	complex	Complex Model
Methyl-tert-butyl ether	complex	Derived from Complex Model Database
2,2,4-Trimethylpentane	simple	
Acrolein	simple	
Ethylbenzene	simple	
n-Hexane	simple	
Propionaldehyde	simple	
Styrene	simple	
Xylene(s)	simple	
Ethanol	simple	

Use of Algorithms Developed for the Complex Model

For the first four compounds listed in Table 5, “complex” toxic fractions were estimated through application of algorithms developed for the Complex Model for Reformulated Gasoline.¹ The equations are based on about 1,800 observations collected on vehicles equipped with three-way or three-way-plus-oxidation catalysts. The algorithms are applied by stratifying the light-duty gasoline fleet into ten Technology Groups and applying the algorithms individually to each group (this formulation is known as the unconsolidated Complex Model). The ten groups are formed as a combination of fuel system, catalyst type, Air injection (yes/no), EGR, and Normal / High emitter status. The first nine groups represent only normal emitting vehicles. The tenth group represents all “high emitters,” regardless of technology. The algorithms are weighted together using model year specific weights obtained from MOBILE6.

The Complex Model algorithms are applied to running, start and extended idle emissions for gasoline fueled vehicles for all 2000 and earlier model years for these four pollutants. While MOBILE6 applied separate equations for older technologies not included in the Complex Model, such as vehicles without catalysts or vehicles with oxidation catalyst, these algorithms were not included in MOVES since these vehicles now comprise such a small portion of the fleet. For 1974 and earlier model years, 1975 weightings are used. In addition, while MOBILE6.2 relied on very limited data from heavy-duty gasoline vehicles, MOVES applies Complex Model algorithms to both light-duty and heavy-duty gasoline vehicles. The general structure of this section and all subsequent ones will be to describe and discuss the calculation algorithms in mathematical terms, show the underlying equation coefficients and present some limited results in graphical form for selected cases

2.1.1.1.1 Overview of the Complex Model

The Complex model is so called because it was designed to model the “complex” behavior of selected emissions in relation to changes in a set of selected fuel properties, so as to facilitate the calculation of “complex fractions,” as defined above.

The underlying dataset included measurements collected on sample of vehicles manufactured in MY1990 or earlier, and reflecting “Tier 0” standards, over a variety of gasoline formulations.

The complex model is composed of sets of models for each pollutant. The models are statistical models fit to sets of emissions measurements on a set of fuels with widely varying properties. For each pollutant, 10 models were fit, with each representing a specific combination of fuel-delivery, catalyst, air injection and emissions-control technology. The technology groups are described in Table 6. As an aggregate, these sets of models are referred to as the “unconsolidated complex model.”

In fitting the complex models, the measurements for all fuel properties were “centered,” meaning that the mean of all measurements for the property was subtracted from each individual measurement. This step aids in scaling the dataset so that each fuel property is centered on a mean of 0.0. Thus, if $\ln Y$ is the natural logarithm of a specific compound, such as acetaldehyde, the model is fit as shown in Equation 1, using terms for oxygenate, sulfur and E300 as examples.

$$\ln Y = \beta_0 + \beta_{\text{oxy}}(x_{\text{oxy},i} - \bar{x}_{\text{oxy}}) + \beta_S(x_{S,i} - \bar{x}_S) + \dots + \beta_{E300}(x_{E300,i} - \bar{x}_{E300}) \quad \text{Equation 1}$$

The mean values used for centering all values are presented in Table 7. Sets of coefficients for models by technology group, are presented for acetaldehyde, formaldehyde, benzene and 1,3-butadiene in Table 8 to Table 11.

Table 6. Technology Groups included in the Complex Model.

Technology Group	Fuel System ¹	Catalyst ²	Air Injection	Exhaust-gas Recirculation
1	PFI	3-Way	No	Yes
2	PFI	3-Way	No	No
3	TBI	3-Way	No	Yes
4	PFI	3-Way + Oxy	Yes	Yes
5	PFI	3-Way	Yes	Yes
6	TBI	3-Way	Yes	Yes
7	TBI	3-Way + Oxy	Yes	Yes
8	TBI	3-Way	No	No
9	carburetor	3-Way + Oxy	Yes	Yes
10 (“High Emitters”)	ALL	ALL	ALL	ALL

¹ Fuel System: PFI= port fuel Injection, TBI= throttle body injection.
² Catalyst type: “3-way”= three-way catalyst, “Oxy”= oxidation catalyst.

Table 7. Mean Fuel-Property Values used for centering Terms in the Complex Models.

Property	Units	Mean Value
Sulfur	ppmW	204.5779
Aromatics	Vol. %	28.26110
Olefins	Vol. %	7.318716
Methyl-tertiary-butyl-ether (MTBE) ¹	Wt.%	0.947240
Ethyl-tertiary-butyl-ether (ETBE) ¹	Wt.%	0.023203
Ethano ¹	Wt.%	0.314352
Tertiary-amyl-methyl-ether (TAME) ¹	Wt.%	0.016443
Oxygenate ²	Wt.%	1.774834
RVP	Psi	8.611478
E200	%	46.72577
E300	%	85.89620

¹ Species-specific values used in the aldehyde models.
² Aggregate value used for the butadiene and benzene models.

Table 8. Complex Model Coefficients for Acetaldehyde, by Technology Group.

Technology Group	Fuel Property									
	Sulfur	Aromatics	Olefins	MTBE	ETBE	EtOH	TAME	RVP	E200	E300
1	0.000263	-0.05548	-	-0.03646	0.316467	0.249326	-	-	-	-0.01216
2	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
3	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
4	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
5	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
6	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
7	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
8	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
9	0.000263	-0.05548	-	-	0.316467	0.249326	-	-	-	-0.01216
10	0.000263	-0.05548	-	-0.05598	0.316467	0.249326	-	-	-	-0.01216

Table 9. Complex Model Coefficients for Formaldehyde, by Technology Group.

Technology Group	Fuel Property									
	Sulfur	Aromatics	Olefins	MTBE	ETBE	EtOH	TAME	RVP	E200	E300
1	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
2	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
3	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
4	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
5	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
6	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
7	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
8	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
9	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023
10	-	-0.00717	-	0.046213	-	-	-	-	-	-0.01023

Table 10. Complex Model Coefficients for Exhaust Benzene, by Technology Group.

Technology Group	Fuel Property							
	Sulfur	Aromatics	Olefins	Oxygenate	Fuel Benzene	RVP	E200	E300
1	0.001054	0.02588	-	-	0.222318	-	-0.00948	-
2	0.000337	0.02588	-	-	0.222318	-	-	-
3	0.001187	0.02588	-	-	0.222318	-	-0.00578	-
4	0.000337	0.02588	-	-	0.222318	-	-	-
5	0.000337	0.04859	-	-	0.222318	-	-	-
6	0.000337	0.02588	-	-	0.222318	-	-	-
7	0.000337	0.02588	-	-	0.222318	-	-	-
8	-	-	-	-	0.222318	-	-	-
9	-0.00195	0.02588	-	-	0.222318	-	-	-
10	0.000337	0.01188	-	-0.09605	0.222318	-	-	0.011251

Table 11. Complex Model Coefficients for 1,3-Butadiene, by Technology Group.

Technology Group	Fuel Property					
	Sulfur	Aromatics	Oxygenate	RVP	E200	E300
1	0.000506	-0.00401	-	-	-0.00731	-0.01678
2	-	-0.00401	-	-	-0.00731	-0.01678
3	0.000544	-0.00401	-	-	-0.00731	-0.01678
4	-0.00041	-0.00401	-	-	-0.00731	-0.01678
5	-	-0.00401	-	-	-0.00731	-0.01678
6	-	-0.00401	-	-	-0.00731	-0.01678
7	-	-0.00401	-	-	-0.00731	-0.01678
8	-	-0.00401	-	-	-0.00731	-0.01678
9	-	-0.00401	-	-	-0.00731	-0.01678
10	-	-0.00401	-0.06077	-	-0.00731	-0.00806

For each compound, the model equations as shown in Equation 1, are evaluated for a “base” and a “target” fuel. The base fuel represents a fuel(s) that corresponds to the emission rates used to calculate the emissions estimates, and which serves as a basis for fuel adjustments. The target fuel is represented by a set of properties from the MOVES database and which represents a fuel “in-use” in the geographic area(s) and season(s) being modeled. <see: signpost to fuel adj doc.>

Initially, an adjustment for the difference in emissions of the compound modeled on the target fuel relative to the base fuel is calculated. If the model, as shown in Equation 1, can be conveniently expressed, using matrix notation, as $X\beta_{\text{target}}$ and $X\beta_{\text{base}}$ for estimates on the target and base fuels, then the fractional difference in emissions is given by

$$f_{\text{adj}} = \frac{\exp(\mathbf{X}\boldsymbol{\beta}_{\text{target}})}{\exp(\mathbf{X}\boldsymbol{\beta}_{\text{base}})} - 1.0 \quad \text{Equation 2}$$

The expression in Equation 2 is evaluated for target and base fuels for each of the ten technology groups. A mean value of the adjustment is then calculated as a weighted average of the values for the groups, with the weights representing the prevalence of each technology combination, as shown in Equation 3. Note that the weights applied to each technology group differ by vehicle age, as shown in Table 12. Note that the use of varying weights in applying the complex model in MOVES differs from the original application in which the weights were invariant.

$$f_{\text{adj,mean}} = \sum_{\text{Group}=1}^{10} w_{\text{Group}} f_{\text{adj,Group}} \quad ; \quad \sum_{\text{Group}=1}^{10} w_{\text{Group}} = 1.0 \quad \text{Equation 3}$$

The mean adjustment calculated in Equation 3 is then applied to estimate the air-toxic emission on the target fuel absent any other adjustments ($E_{\text{relative,toxic}}$), while incorporating the effect on the emissions of the toxic due to the changes in fuel properties between the target and base fuels. If the target and base fuels were identical, the value of $f_{\text{adj,mean}}$ would be 0.0.

$$E_{\text{relative,toxic}} = E_{\text{base,toxic}} (1 + f_{\text{adj,mean}}) \quad \text{Equation 4}$$

The values of $E_{\text{relative,toxic}}$ are the air toxic emission rates in units of grams per mile, and are a function of month of the year. They were taken directly from the Complex Model Spreadsheet “*CM Final.xls*”. They are the base air-toxic emissions for the Base Fuel in the air toxics model. These base emissions were calculated from air toxic emission data from the Tier 0 vehicles in the original air toxic / fuel effects studies on which the Complex Model was based.

The calculations in Equation 1 to Equation 4 are also applied to VOC Emissions, ending with the generation of a value of $E_{\text{relative,VOC}}$. This value for VOC is then combined with that for each toxic to calculate a fraction used to estimate the total mass of emissions for each toxic during a model run. These fractions are denoted as f_{toxic} and calculated as shown in Equation 5.

$$f_{\text{toxic}} = \frac{E_{\text{relative,toxic}}}{E_{\text{relative,VOC}}} \quad \text{Equation 5}$$

As a final step, the mass emissions of each toxic during a model run are estimated by multiplying the mass of VOC emissions estimated by MOVES I_{VOC} by the values of f_{toxic} .

$$I_{\text{toxic}} = f_{\text{toxic}} I_{\text{VOC}}$$

Equation 6

Note that the algorithm as described here is based on an assumption that within each technology group, the relations of air-toxic emissions to changes in fuel properties has remained stable as emissions standards transitioned from Tier 0 to Tier 1 levels.

Table 12. Weights Applied to Complex Model coefficients for Technology Groups, by Age.^a

Age	Technology Group									
	1	2	3	4	5	6	7	8	9	10
0	0.2360	0.2829	0.1806	0.1814	0.0290	0.0042	0.0556	0.0	0.0203	0.0100
1	0.2339	0.2803	0.1789	0.1797	0.0287	0.0042	0.0551	0.0	0.0201	0.0190
2	0.2315	0.2774	0.1771	0.1779	0.0284	0.0041	0.0546	0.0	0.0199	0.0290
3	0.2272	0.2723	0.1738	0.1746	0.0279	0.0041	0.0536	0.0	0.0196	0.0470
4	0.2229	0.2672	0.1706	0.1713	0.0274	0.0040	0.0525	0.0	0.0192	0.0650
5	0.2189	0.2623	0.1675	0.1682	0.0269	0.0039	0.0516	0.0	0.0188	0.0820
6	0.2148	0.2574	0.1644	0.1651	0.0264	0.0038	0.0506	0.0	0.0185	0.0990
7	0.2110	0.2529	0.1614	0.1621	0.0259	0.0038	0.0497	0.0	0.0182	0.1150
8	0.2072	0.2483	0.1585	0.1592	0.0254	0.0037	0.0488	0.0	0.0178	0.1310
9	0.2036	0.2440	0.1558	0.1565	0.0250	0.0036	0.0480	0.0	0.0175	0.1460
10	0.2000	0.2397	0.1530	0.1537	0.0246	0.0036	0.0471	0.0	0.0172	0.1610
11	0.1967	0.2357	0.1505	0.1512	0.0241	0.0035	0.0464	0.0	0.0169	0.1750
12	0.1934	0.2317	0.1479	0.1486	0.0237	0.0035	0.0456	0.0	0.0166	0.1890
13	0.1903	0.2280	0.1456	0.1462	0.0234	0.0034	0.0448	0.0	0.0164	0.2020
14	0.1872	0.2243	0.1432	0.1438	0.0230	0.0033	0.0441	0.0	0.0161	0.2150
15	0.1843	0.2209	0.1410	0.1416	0.0226	0.0033	0.0434	0.0	0.0159	0.2270
16	0.1814	0.2174	0.1388	0.1394	0.0223	0.0032	0.0428	0.0	0.0156	0.2390
17	0.1786	0.2140	0.1366	0.1372	0.0219	0.0032	0.0421	0.0	0.0154	0.2510
18	0.1760	0.2109	0.1346	0.1352	0.0216	0.0031	0.0415	0.0	0.0151	0.2620
19	0.1736	0.2080	0.1328	0.1334	0.0213	0.0031	0.0409	0.0	0.0149	0.2720
20	0.1712	0.2052	0.1310	0.1315	0.0210	0.0031	0.0403	0.0	0.0147	0.2820
21	0.1688	0.2023	0.1291	0.1297	0.0207	0.0030	0.0398	0.0	0.0145	0.2920
22	0.1664	0.1994	0.1273	0.1279	0.0204	0.0030	0.0392	0.0	0.0143	0.3020
23	0.1643	0.1969	0.1257	0.1262	0.0202	0.0029	0.0387	0.0	0.0141	0.3110
24	0.1624	0.1946	0.1242	0.1248	0.0199	0.0029	0.0383	0.0	0.0140	0.3190
25	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280
26	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280
27	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280
28	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280
29	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280
30	0.1602	0.1920	0.1226	0.1231	0.0197	0.0029	0.0378	0.0	0.0138	0.3280

a. Note that in the MOVES database, these weights are stored in the table FuelModelWtFactor.

2.1.1.1.2 Estimating Emissions of Methyl-tertiary-butyl-ether (MTBE)

As of calendar year 2008, MTBE (pollutantID = 22) has been almost completely phased-out of the fuel supply of the United States due to concerns related to contamination of ground water. Thus, its inventory levels in the MOVES output from default inputs should be very small if not zero in future years. It is present in the MOVES model as mostly a legacy pollutant for calendar years 1990 and 1999 – 2005. However, the MTBE fuel volume is a user input, and MOVES has the capability to calculate MTBE emissions for any calendar year.

For MTBE, a fuel-effects model based on the Complex Model database and applied in MOBILE6.2 was used.^{2,3} This model is based on algorithms from underlying data of nearly 900 observations. However, instead of using model equations directly, MOBILE6.2 was run at different fuel MTBE volumes (V_{MTBE}). Using the results, MTBE fractions were calculated and related to MTBE levels using simple regression. A quadratic equation fixed at the origin was found to give the best fit. This curve was then used in MOVES. The equation is shown in Equation 7 and the parameters are shown in Table 1. The same equation is used for both start and running processes and is shown in Equation 7.

$$f_{MTBE} = AV_{MTBE} + BV_{MTBE}^2 \quad \text{Equation 7}$$

The coefficients A and B take the values shown in Table 13. As with the other toxic emissions, the fraction f_{MTBE} is multiplied by the mass of VOC to estimate MTBE emissions, as shown in Equation 6.

Table 13. Exhaust Calculation Coefficients for MTBE (see Equation 7).

Pollutant Process	polProcessID	A (coeffA)	B (coeffB)
Running Exhaust	2201	0.00007809	0.00007537
Start Exhaust	2202	0.00007809	0.0007809

It should be noted that the sulfur effects terms in the equations were not included; rather, sulfur effects on toxic emissions were assumed to be proportional to the sulfur impacts on total VOC estimated by MOVES.

Data were not available to develop algorithms for ETBE and TAME blends; thus, the algorithms for ethanol oxygenated gasoline were used for ETBE blends, and the algorithms for MTBE oxygenated gasoline were used for MTBE blends.

2.1.1.1.3 Simple Fractions

Table 14 lists toxic fractions for a set of additional hydrocarbons designed to represent toxic emissions for several fuel blends containing different oxygenates. For gasoline fuels containing 0 and 10% ethanol (E0 and E10), fractions were developed by Sierra Research using speciation profiles estimated from EPA's SPECIATE 4.2 database.⁴ The fractions for E10 are also used to represent blends in which the oxygenate is ethyl-tertiary-butyl-ether (ETBE) at levels of 5 vol.% or greater.

For blends containing methyl-tertiary-butyl ether (MTBE), however, fractions were adopted from National County Database for the National Mobile Inventory Model (NMIM). The fractions used in NMIM were derived for the 1999 National Emission Inventory (NEI) for

HAPS, version 3, and summarized in Volume 1, Appendix D, Table 1 of the documentation. These ratios were based on older speciation profiles than the E0 and E10 data. One set of fractions represents winter fuels containing MTBE at 12 vol. % or more, or tertiary-amy-l-methyl-ester (TAME) at levels of 13% or more (winter). A second set represents reformulated gasoline fuels containing MTBE at levels between 5.0 and 13.0 vol.% or TAME at levels between 5.0 and 13.0 vol.% (RFG). Separate ratios are used for each of the following four categories of gasoline blends:

Emissions of ethanol in exhaust are estimated for gasoline blends containing ethanol at levels of 0 to 10 vol.%. For vehicles running on 10% ethanol, ethanol was estimated to comprise 2.39% of exhaust VOC. This estimate is based on results measured on nine vehicles in four test programs.^{5, 6, 7, 8} The fraction of ethanol in exhaust VOC for blends containing 5.0% and 8.0% ethanol is estimated by interpolating linearly between the fractions for 0.0% and 10.0% ethanol. No data exist for 2000 and earlier vehicles running on E15 or E20. Thus, toxics ratios for 2001 and later vehicles are used.

Table 14. Toxic Fractions for Selected Air Toxics, Representing Gasoline and Ethanol Blends (“Gasohol”).

Compound	pollutantID	Fuel Blend (by Ethanol Level)	
		0% (E0)	10% (E10)
2,2,4-Trimethylpentane	40	0.01823	0.01849
Acrolein		0.0006	0.0006
Ethyl Benzene	41	0.02147	0.01932
n-Hexane	42	0.01570	0.01593
Propionaldehyde	43	0.00086	0.00086
Styrene	44	0.00108	0.00097
Toluene	45	0.09619	0.08657
Xylene	46	0.07814	0.07032
Ethanol			0.0239

Table 15. Toxic Fractions for Selected Air Toxics , Representing Gasolines containing MTBE.

Compound	pollutantID	MTBE	
		Winter	RFG
2,2,4-Trimethylpentane	40	0.04327	0.04327
Acrolein		0.0006	0.0006
Ethyl Benzene	41	0.01398	0.01484
n-Hexane	42	0.00861	0.00888
Propionaldehyde	43	0.00073	0.00073
Styrene	44	0.00328	0.00340
Toluene	45	0.09873	0.10494
Xylene	46	0.05557	0.05910

In the MOVES database, these inputs are stored in the table “minorHAPratio.” In the label, the term “HAP” refers to “hazardous air pollutant.” A description of the table is provided in Table 16.

Table 16. Description of the Database Table “minorHAPRatio.”

Field	Description	RelevantValues
polProcessID	Identifies the pollutant (1 st two digits and Emissions Process (last two digits).	Pollutants are identified in the table above; Relevant processes include: “Running Exhaust” (processID = 1) “Start Exhaust” (processID = 2)
fuelTypeID	Identifies broad classes of fuels, e.g., “gasoline.” “diesel.”	1 = “Gasoline” 2 = “Diesel” 5 = “Ethanol”
fuelSubTypeID	Identifies specific fuel classes within the fuelTypeID	10 = “Conventional Gasoline” 11 = “Reformulated Gasoline” 12 = “Gasohol (E10)” 13 = “Gasohol (E8)” 14 = “Gasohol (E5)” 15 = “Gasohol (E15)” 18 = “Gasohol (E20)” 51 = “Ethanol (E85)” 52 = “Ethanol (E70)”
modelYearGroupID	Identifies a set of model years covered by a specific value of atRatio.	1960-1970 1971-1977 1978-1995 1996-2003 2004-2050
atRatio	Fraction, or “ratio” of the toxic relative to total VOC.	
atRatioCV	“Coefficient of Variation of the Mean” or “relative standard error” of the atRatio.	
dataSourceID	Indicates source data and methods used to estimate atRatio.	

2.1.1.2 Vehicles operating on Fuel blends containing 70-100% Ethanol

Toxic fractions for vehicles running on fuels containing 70-100% ethanol were derived from measurements on four flexible fuel vehicles, conducted during the EPA Act program (Phase 3). The vehicles were tested on a single E85 gasoline. Since no tests were done on an E70 blend, more typically used in winter and blends above E85, the same toxic to VOC ratios are used for blends containing 70-100% ethanol.

Of the fractions shown in Table 17, those with pollutantID from 40-46 are stored in the database table “minorHAPRatio” (see Table 16, page 19). Those with pollutantID from 20-27 are stored in the database table “ATRatioNonGas” (see Table 18).

Table 17. Toxic Fractions for vehicles running on E70/E85

Pollutant (pollutantID)	Toxic Fraction
2,2,4-Trimethylpentane (40)	0.0078
Ethyl Benzene (41)	0.0055
Hexane (42)	0.0045
Propionaldehyde (43)	0.0025
Styrene (44)	0.0003
Toluene (45)	0.0177
Xylene(s) (46)	0.0185
1,3-Butadiene (24)	0.0011
Acetaldehyde (26)	0.1644
Acrolein (27)	0.0010
Benzene (20)	0.0170
Ethanol (21)	0.3724
Formaldehyde (25)	0.0291

Table 18. Description of the Database Table “ATRatioNonGas,” as Applied to Light-Duty Vehicles.

Field	Description	RelevantValues
polProcessID	Identifies the pollutant (1 st two digits and Emissions Process (last two digits).	Pollutants are identified in the table above; Relevant processes include: “Running Exhaust” (processID = 1) “Start Exhaust” (processID = 2) “Extended Idle Exhaust” (processID = 90) “Auxiliary Power Exhaust” (processID = 91)
sourceTypeID	Identifies types of vehicles, classified by function	Motorcycle (11) Passenger Car (21) Passenger Truck (31) Light Commercial Truck (32)
fuelSubTypeID	Identifies specific fuel classes within the fuelTypeID	51 = “Ethanol (E85)” 52 = “Ethanol (E70)”
modelYearGroupID	Identifies a set of model years covered by a specific value of atRatio.	
atRatio	Fraction, or “ratio” of the toxic relative to total VOC.	
atRatioCV	“Coefficient of Variation of the Mean” or “relative standard error” of the atRatio.	
dataSourceID	Indicates source data and methods used to estimate atRatio.	

2.1.2 Polycyclic Aromatic Hydrocarbons (PAH)

Emissions of PAH are estimated through the use of fractions in a manner similar to that used for gaseous hydrocarbons as described in the previous section. However, for PAH, the process is complicated by the fact that these compounds are emitted in both the gaseous and particulate phases. Accordingly, emissions in the gaseous phase are estimated as fractions of total VOC, and emissions in the particulate phase as fractions of organic carbon (less than 2.5 microns in diameter, OC_{2.5}), as ratios to the VOC and OC_{2.5} exhaust and crankcase emissions.

The fractions are estimated from a set of 99 vehicles measured in the Kansas City Light-duty Vehicle Emissions Study (KCVES)⁹. These vehicles were included in a subsample selected for chemical speciation. For each vehicle, emissions of total hydrocarbons (THC) and PM_{2.5} were measured. Fleet-average fractions of PAH/THC and PAH/PM_{2.5} were calculated with each sample weighted according to total emissions, vehicle-miles traveled (VMT), and an equal weight between summer and winter.¹⁰ We used the THC measurements to represent VOC emission rates, and we corrected the PAH/PM_{2.5} by the fraction of OC measured in the start (42.6%) and running emission processes (55.7%) to produce PAH/OC_{2.5} emission rates¹⁰. At this stage in the analysis, the PAHs are not allocated to gas or particle phase. The next paragraphs discuss how these fractions were then adjusted to allocate the PAHs to the gaseous or particle phases.

The true gas-particle partitioning of PAHs emissions in the atmosphere depends on particle and gas concentrations, exhaust temperature and other factors. However, in preparing inputs for MOVES, we developed one set of allocation factors for gasoline sources and another for diesel sources under all conditions in order to streamline data processing, and to be consistent with the PAH data as measured in test programs. The sampling conditions set forth in EPA regulations for particulate and hydrocarbons differ for light-duty and heavy-duty vehicles which impacts the phase partitioning of the PAH emissions.

The allocations of PAH into gaseous and particulate phases are based on measurement samples analyzed by Desert Research Institute (DRI) on a subset of vehicles in the KCVES that were measured with dilution air at both low and high temperatures.¹¹ One of the purposes of this follow-up study was to examine the impact of sampling conditions on PAH emission measurements. DRI measured PAH species with Teflon-impregnated glass filters (TIGF) and backup glass cartridges with Amberlite XAD-4 adsorbent resins over the LA-92 cycle. Relative concentrations of individual PAH were measured on the TIGF and the XAD with dilution temperatures of 20°C and 47°C for four composite samples of vehicles. Table 19 reports the TIGF/XAD phase allocation factors measured at 47°C (which was the measurement temperature for the Kansas City Light-duty Vehicle Emissions Study), for the composite class referred to as the 'medium-emitters.' This class contained a 1989 Camry and 1992 Voyager. In MOVES2014, we used the PAH phase-partitioning of this sample to estimate the relative gas and particle partitioning of all gasoline-source emissions. Note that the PAH species partitioning was heavily dependent on molar mass (molecular weight); compounds with the smallest molar masses (e.g., naphthalene) were measured almost entirely in the gaseous phase, whereas compounds with the highest molar masses were measured almost entirely in the particulate phase (e.g. dibenzo(a,h)anthracene).

Table 19. Gasoline PAH phase allocation factors.

PAH species	Molar Mass (g/mol)	Phase Fraction	
		Gaseous	Particulate
Naphthalene	128	0.9996	0.0004
Acenaphthylene	152	0.9985	0.0015
Acenaphthene	154	1.0000	0.0000
Fluorene	166	1.0000	0.0000
Anthracene	178	0.9915	0.0085
Phenanthrene	178	0.9953	0.0047
Fluoranthene	202	0.9822	0.0178
Pyrene	202	0.9831	0.0169
Benz(a)anthracene	228	0.6721	0.3279
Chrysene	228	0.7307	0.2693
Benzo(a)pyrene	252	0.0426	0.9574
Benzo(b)fluoranthene	252	0.5546	0.4454
Benzo(k)fluoranthene	252	0.5546	0.4454
Benzo(g,h,i)perylene	276	0.0000	1.0000
Indeno(1,2,3-cd)pyrene	276	0.0000	1.0000
Dibenzo(a,h)anthracene	278	0.0000	1.0000

We multiplied the phase allocation factors in Table 19 by the PAH/VOC and PAH/OC2.5 ratios from the KCVES to obtain the ratios in Table 20 used in MOVES2014. These ratios are applied to all gasoline fuels with ethanol content less than 20%. In the MOVES database, these fractions are stored in two tables. Fractions for the gaseous phase are stored in the table “pahgasratio” and those for the particulate phase are stored in the table “pahparticleratio.” The two tables have the same structure which is presented in Table 20.

Table 20. Toxic Fractions for PAH Compounds, in Gaseous and Particulate Phases.

PAH species	pollutantID	CAS	Fraction (PAH/VOC)	Fraction (PAH/OC _{2.5})	
				Start	Running
Naphthalene	23	91203	1.77E-03	1.68E-04	1.29E-04
Acenaphthylene	42	208968	1.55E-04	5.01E-05	3.83E-05
Acenaphthene	41	83329	3.41E-05	0E+00	0E+00
Fluorene	54	86737	6.91E-05	0E+00	0E+00
Anthracene	44	120127	2.86E-05	5.19E-05	3.97E-05
Phenanthrene	57	85018	1.83E-04	1.81E-04	1.39E-04
Fluoranthene	53	206440	4.79E-05	1.83E-04	1.40E-04
Pyrene	59	129000	5.47E-05	1.98E-04	1.52E-04
Benz(a)anthracene	45	56553	4.62E-06	4.76E-04	3.64E-04
Chrysene	50	218019	5.17E-06	4.02E-04	3.08E-04
Benzo(a)pyrene	46	50328	2.52E-07	1.19E-03	9.13E-04
Benzo(b)fluoranthene	47	205992	3.43E-06	5.81E-04	4.45E-04
Benzo(k)fluoranthene	49	207089	3.43E-06	5.81E-04	4.45E-04
Benzo(g,h,i)perylene	48	191242	0E+00	3.23E-03	2.47E-03
Indeno(1,2,3,c,d)pyrene	56	193395	0E+00	1.21E-03	9.28E-04
Dibenzo(a,h)anthracene	51	53703	0E+00	2.79E-05	2.13E-05

2.1.3 Metals

Emissions of metals in vehicle exhaust result from trace-level contamination of fuel and engine oil, as well as attrition from engine, exhaust system, and emission control components. MOVES estimates metal emissions for five metal species, including two valence forms of chromium and 3 forms of mercury, using emission rates expressed on a distance-specific basis (g/mile). Emission rates for chromium, magnesium and nickel are developed from the 99 vehicles sampled for chemical composition in the KCVES. The average g/mile rates are calculated by averaging the metal measured on bag 2 of the LA-92, with a weighted-average computed to be representative of the on-road vehicle fleet.¹⁰ We used bag 2, so the emission rates for these metals are consistent with the PM_{2.5} emission profile for running gasoline discussed in the MOVES2014 TOG and PM Speciation Report. PM_{2.5} emissions are much more enriched in metals during hot-stabilized running conditions than during start emissions. We compared the g/mi emission rates from bag 2 to the average of the entire LA-92; the difference in the bag 2 emission rates from the average of the LA-92 is 38%, -2% and -16% for manganese, chromium, and nickel. Thus, in using bag 2 emission rates for metal emission rates we are both consistent with the PM_{2.5} speciation running emission profile, and conservative when compared to using the cycle average.

Eighteen percent of chromium was assumed to be hexavalent, based on combustion data from stationary combustion turbines burning diesel fuel.¹² Emission factors for arsenic were developed from data reported for tunnel tests.¹³ Emission factors for mercury were obtained from

a 2005 EPA test program. Documentation describing development of these emission factors can be found in Appendix A. Metal emission rates do not vary among fuel types. Rates are presented in Table 21. These values are stored in the database table “metalEmissionRate,” which is described in Table 22.

Table 21. Metal emission Rates for gasoline vehicles and trucks.

Pollutant	Emission Rate (g/mi)
Chromium, hexavalent (6+)	7.32E-07
Chromium, trivalent (3+)	3.34E-06
Manganese	1.33E-06
Nickel	1.50E-06
Mercury, Elemental (Gaseous Phase)	1.10E-07
Mercury, Reactive (Gaseous Phase)	9.90E-09
Mercury, Particulate Phase	4.00E-10
Arsenic	2.30E-06

Table 22. Description of the Database Table “metalEmissionRate.”

Field	Description	RelevantValues
polProcessID	Identifies the pollutant (1 st two digits and Emissions Process (last two digits).	Pollutants are identified in the table above; Relevant processes include: 1 = “Running Exhaust”
fuelTypeID	Identifies broad classes of fuels, e.g., “gasoline.” “diesel.”	1 = “Gasoline” 2 = “Diesel” 5 = “Ethanol”
sourceTypeID	Identifies vehicle types, classified by function	Motorcycles (11) Passenger Cars (21) Passenger Trucks (31) Light Commercial Trucks (32)
modelYearGroupID	Identifies a set of model years covered by a specific value of atRatio.	1960-1970 1971-1977 1978-1995 1996-2006 2007-2050
Units	Identifies units in which the meanBaseRate is expressed.	grams/mile
meanBaseRate	Average emission rate for a combination of process, fuel type, sourceType and modelYearGroup.	
meanBaseRateCV	“Coefficient of Variation of the Mean” or “relative standard error” of the meanBaseRate.	
dataSourceID	Indicates source data and methods used to estimate atRatio.	

2.1.4 Dioxins and Furans

MOVES estimates emissions for 17 dioxin and furan congeners in mg/mi toxic equivalents (TEQs). The emissions are estimated using distance-specific emission rates multiplied by World Health Organization 2005 toxic equivalency factors (TEFs; Table 23).¹⁴ Thus, emission rates for the various congeners are expressed as TEQs of the most toxic congener (2,3,7,8 TCDD)(Table 23)These emission factors were obtained from a tunnel study and used in EPA’s dioxin assessment.^{15,16} They do not vary among fuel types. The rates are stored in the database table “dioxinEmissionRate,” which is described in Table 25.

Table 23. Dioxin/Furan Toxic Equivalency Factors (World Health Organization)

Pollutant	TEF
2,3,7,8-TCDD TEQ	1.0
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	1.0
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	0.10
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	0.10
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	0.10
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	0.01
Octachlorodibenzo-p-dioxin	0.0003
2,3,7,8-Tetrachlorodibenzofuran	0.10
1,2,3,7,8-Pentachlorodibenzofuran	0.030
2,3,4,7,8-Pentachlorodibenzofuran	0.3
1,2,3,4,7,8-Hexachlorodibenzofuran	0.1
1,2,3,6,7,8-Hexachlorodibenzofuran	0.1
1,2,3,7,8,9-Hexachlorodibenzofuran	0.1
2,3,4,6,7,8-Hexachlorodibenzofuran	0.1
1,2,3,4,6,7,8-Heptachlorodibenzofuran	0.01
1,2,3,4,7,8,9-Heptachlorodibenzofuran	0.01
Octachlorodibenzofuran	0.0003

Table 24. Dioxin emission Rates for gasoline vehicles.

Pollutant	TEQ (mg/mi)
2,3,7,8-Tetrachlorodibenzo-p-Dioxin (TCDD)	8.27E-10
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	3.70E-10
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	3.87E-11
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	7.92E-11
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	4.93E-11
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	5.95E-11
Octachlorodibenzo-p-dioxin	1.41E-11
2,3,7,8-Tetrachlorodibenzofuran	2.76E-10
1,2,3,7,8-Pentachlorodibenzofuran	3.96E-11
2,3,4,7,8-Pentachlorodibenzofuran	2.90E-10
1,2,3,4,7,8-Hexachlorodibenzofuran	1.09E-10
1,2,3,6,7,8-Hexachlorodibenzofuran	1.16E-10
1,2,3,7,8,9-Hexachlorodibenzofuran	3.17E-11
2,3,4,6,7,8-Hexachlorodibenzofuran	1.36E-10
1,2,3,4,6,7,8-Heptachlorodibenzofuran	1.21E-10
1,2,3,4,7,8,9-Heptachlorodibenzofuran	3.87E-12
Octachlorodibenzofuran	4.11E-12

Table 25. Description of the Database Table “DioxinEmissionRate.”

Field	Description	RelevantValues
polProcessID	Identifies the pollutant (1 st two digits and Emissions Process (last two digits).	Pollutants are identified in the table above; Relevant processes include: 1 = “Running Exhaust”
fuelTypeID	Identifies broad classes of fuels, e.g., “gasoline.” “diesel.”	1 = “Gasoline” 2 = “Diesel” 5 = “Ethanol”
modelYearGroupID	Identifies a set of model years covered by a specific value of atRatio.	1960-2050 1960-2006 2007-2009 2010-2050
Units	Identifies units in which the meanBaseRate is expressed.	grams/mile
meanBaseRate	Average emission rate for a combination of process, fuel type, sourceType and modelYearGroup.	
meanBaseRateCV	“Coefficient of Variation of the Mean” or “relative standard error” of the meanBaseRate.	
dataSourceID	Indicates source data and methods used to estimate atRatio.	

2.2 Light-Duty Vehicles (gasoline powered): Model-year 2001 and later

For vehicles manufactured in MY2001 and later, and certified to NLEV or Tier 2 standards, recently collected data was available. As before, toxic emissions are estimated as fractions of VOC, with toxic fractions for various compounds estimated using differing datasets and methods. For some compounds and processes, models were developed to estimate “complex” fractions (responding to fuel properties), whereas for others, “simple” fractions were estimated (not responding to fuel properties). An additional feature for these fractions is that in some cases, different fractions could be estimated for the start and running emission processes. For the compounds included in MOVES, data sources and estimation methods are summarized in Table 26.

Table 26. Data Sources and Estimation Methods Used in Estimation of Toxic Fractions for Gaseous Hydrocarbons.

Compound	Process	Fraction Type	Basis for Estimation
Acetaldehyde	Start	complex	application of EPAct models
	Running	complex	application of EPAct models ¹
Formaldehyde	Start	complex	application of EPAct models
	Running	complex	application of EPAct models
Acrolein	Start	complex	application of EPAct models
	Running	simple	Data from EPAct Project (Phase 3) ²
Ethanol	Start	complex	application of EPAct models
	Running	complex	application of EPAct models
Benzene	Start	complex	application of EPAct models
	Running	simple	Data from EPAct Project (Phase 3)
1,3-Butadiene	Start	complex	application of EPAct models
	Running	simple	Data from EPAct Project (Phase 3)
2,2,4-Trimethylpentane	Both	simple	Speciation Profile (EPAct Phase 1) ³
Ethylbenzene	Both	simple	Speciation Profile (EPAct Phase 1)
N-Hexane	Both	simple	Speciation Profile (EPAct Phase 1)
Propionaldehyde	Both	simple	Speciation Profile (EPAct Phase 1)
Styrene	Both	simple	Speciation Profile (EPAct Phase 1)
Xylene(s)	Both	simple	Speciation Profile (EPAct Phase 1)
¹ Derived from models fit to data from EPAct Phase 3 Results. ² Derived from data collected in EPAct Phase 3. ³ Derived from data collected in EPAct Phase 1.			

2.2.1 Application of the Results of the EPAct Program

An important function of mobile source air pollution inventory models, including MOBILE6 and MOVES, is to account for the effects of different fuel properties on exhaust emissions. For this purpose, MOBILE6 relied on previously existing fuel-effect models, known as the ‘EPA Predictive Model’ and the ‘Complex Model’. While these models are still in use in MOVES to estimate fuel effects for vehicles manufactured prior to model year 2001 their applicability to vehicles employing more recent engine and emission control technologies has been questioned. Since the initiation of the MOVES project, it has become clear that an updated fuel-effects model representing Tier-2 certified vehicles would be needed. In addition, Congress provided for the development of such a model in the 2005 Energy Policy Act (EPAct).

To meet this goal, EPA entered a partnership with the Department of Energy (DOE) and the Coordinating Research Council (CRC) to undertake the largest fuels research program conducted since the Auto/Oil program in the early 1990’s, aimed specifically at understanding the effects of fuel property changes on exhaust emissions on recently manufactured Tier 2 vehicles. The

resulting research program was dubbed the “EPAct/V2/E-89” program (or “EPAct” for short), with the three components of the label denoting the designation given to the study by the EPA, DOE and CRC, respectively.

The program was conducted in three phases. Phases 1 and 2 were pilot efforts involving measurements on 19 light-duty cars and trucks on three fuels, at two temperatures. These preliminary efforts laid the groundwork for design of a full-scale research program, designated as Phase 3.

Initiated in March 2009, the Phase 3 program involved measurement of exhaust emissions from fifteen high-sales-volume Tier-2 certified vehicles (model year 2008), using twenty-seven test fuels spanning wide ranges of five fuel properties (ethanol, aromatics, vapor pressure, and two distillation parameters: T50 and T90). The properties of the test fuels were not assigned to represent in-use fuels, but rather to allow development of statistical models that would enable estimation of relative differences in emissions across the ranges of fuel properties expected in the U.S. fuel pool. A fuel matrix was designed for Phase 3 to span the ranges of the five selected properties seen in commercially available fuels.

An initial sample of 19 test vehicles was chosen with the intent of representing the latest-technology light-duty vehicles being sold at the time the program was launched (model year 2008). The 19 vehicles represented a high fraction of vehicle sales at the time. The sample was to conform on average to Tier-2 Bin-5 exhaust levels and employ a variety of emission control technologies, to be achieved by including a range of vehicle sizes and manufacturers. Due to budget constraints, the sample was reduced from 19 to 15 vehicles for the Phase-3 program.

The LA92 test cycle was used with emissions measured over three phases analogous to those in the Federal Test Procedure (FTP), at an ambient temperature of 75°F. In MOVES, the EPAct results are applied at temperatures higher and lower than this level, under an assumption that effects for fuels and temperature are independent and multiplicative.

Emissions measured include carbon dioxide (CO₂), carbon monoxide (CO), total hydrocarbons (THC), methane (CH₄), oxides of nitrogen (NO_x), and particulate matter (PM_{2.5}). In addition, hydrocarbons were speciated for subsets of vehicles and fuels, allowing calculation of derived parameters such as non-methane organic gases (NMOG) and non-methane hydrocarbons (NMHC). Speciation also allowed independent analyses of selected toxics including acetaldehyde, formaldehyde, acrolein, benzene and 1,3-butadiene.

Phase 3 data collection was completed in June 2010. Dataset construction and analysis was conducted between January 2010 and November 2012. This process involved ongoing collaboration among EPA staff, DOE staff and contractors, and CRC representatives. Following the completion of data collection, construction of the dataset involved intensive evaluation and quality assurance. The analysis involved several iterations between analysis and additional physical and chemical review of the data. Successive rounds of statistical modeling were applied to the data, to achieve several goals, including identification of potential candidate models, identification and review of outlying observations, identification and review of subsets of data from influential vehicles, and identification of models including subsets of terms that best explain the results obtained.

The EPAct exhaust research program and analysis are extensively documented in the “EPAct Test Program Report¹⁷” and “EPAct Analysis Report.¹⁸”

This document describes how the data and statistical models developed during the EPAct study are applied in the MOVES model (MOVES2014).

2.2.1.1 Standardizing Fuel Properties

In applying the EPAct models to estimate emissions effects for a given fuel, it is necessary to first “center” and “scale” the properties for the fuel, also known as “standardization.” This process simply involves first “centering” the measured fuel properties by subtracting the given value from the sample mean, and then “scaling” by then dividing the centered values by their respective standard deviations, as shown in Equation 8. Note that the means and standard deviations are calculated from the fuel set used for the program (see Table 26, page 28). The result is a “Z score,” representing a “standard normal distribution” with a mean of 0.0 and a standard deviation of 1.0.

$$Z_i = \frac{x_i - \bar{x}}{s} \quad \text{Equation 8}$$

For the linear effects in the model, standardization is performed using the values of each fuel property, each in their respective scales (vol. %, psi, °F.). Using aromatics as an example, the standardization of the linear term is shown in Equation 9.

$$Z_{\text{arom}} = \frac{x_{\text{arom}} - \bar{x}_{\text{arom}}}{s_{\text{arom}}} \quad \text{Equation 9}$$

For second-order terms, however, the process is not performed on the values of the fuel properties themselves. Rather, quadratic and interaction terms are constructed from the Z scores for the linear terms, and the process is repeated. Using the quadratic term for ethanol as an example (etOH×etOH), the standardized value, denoted by $ZZ_{\text{etOH} \times \text{etOH}}$, is calculated as shown in Equation 10, where $m_{Z_{\text{etOH}}Z_{\text{etOH}}}$ and $s_{Z_{\text{etOH}}Z_{\text{etOH}}}$ are the mean and standard deviation of the quadratic term constructed from the Z score for the linear effect.

$$ZZ_{\text{etOH} \times \text{etOH}} = \frac{Z_{\text{etOH}}Z_{\text{etOH}} - m_{Z_{\text{etOH}}Z_{\text{etOH}}}}{s_{Z_{\text{etOH}}Z_{\text{etOH}}}} \quad \text{Equation 10}$$

Standardized terms for interaction effects are constructed similarly. For example, Equation 11 shows the standardization of an interaction term between ethanol and aromatics.

$$ZZ_{\text{etOH}\times\text{Arom}} = \frac{Z_{\text{etOH}}Z_{\text{Arom}} - m_{Z_{\text{etOH}}Z_{\text{Arom}}}}{s_{Z_{\text{etOH}}Z_{\text{Arom}}}} \quad \text{Equation 11}$$

2.2.1.2 Application of EPAct Statistical Models

The approach for toxics estimates the emissions of the toxic as a fraction of emissions for VOC, on the same fuel. So, to model the behavior of the fraction with respect to changes in fuel properties, it was necessary to develop models for NMOG and Ethane, as well as the toxics, because MOVES estimates VOC as NMOG minus Ethane.

The models generated using EPAct results allow estimation of emissions effects related to five fuel properties: ethanol content (vol.%), aromatics content (vol.%), RVP (psi), T50 (°F) and T90 (°F), as well as selected interaction terms among these five parameters. The statistical models generated from the EPAct exhaust data follow the general structure shown in Equation 12 below. In this example equation, β denotes a model coefficient, Z_{etOH} denotes a “standardized” fuel term for this property, and $Z_{\text{etOH}\times\text{Arom}}$ denotes a “standardized” etOH×Arom interaction term.^b For simplicity, the terms for ethanol and the etOH×Arom interaction have been shown; linear and interaction terms for the remaining three properties are not shown in this example. Finally, the term s_e^2 represents the residual error or “mean square error” for the model. Note that the subsets of the potential terms vary by emission and process, depending on the results of the statistical model fitting.

When the data was sufficient, two sets of exhaust fuel effect coefficients were employed for each pollutant; one set representing start emissions and a second set representing hot-running emissions. In some cases fuel effects estimated for these two processes differed substantially, as the effects of fuel properties on start emissions are dominated by changes in combustion and catalyst warm-up, while the impact of running emissions is dictated by catalyst efficiency when fully operational.

$$\begin{aligned} \text{Emissions (g/mi)} &= e^{\mathbf{X}\boldsymbol{\beta}} \\ &= \exp\left(\beta_0 + \beta_{\text{etOH}}Z_{\text{etOH}} + [\text{other linear terms}] + \beta_{\text{etOH}\times\text{Arom}}Z_{\text{etOH}\times\text{Arom}} + \right. \\ &\quad \left. [\text{other 2nd-order terms}] + 0.5s_e^2 \right) \quad \text{Equation 12} \end{aligned}$$

Thus, if we let $\mathbf{X}\boldsymbol{\beta}_{\text{toxic}}$, $\mathbf{X}\boldsymbol{\alpha}_{\text{NMOG}}$ and $\mathbf{X}\boldsymbol{\theta}_{\text{ethane}}$ represent models for a selected toxic compound, NMOG and ethane, respectively, calculated by applying Equation 12 to each compound for a specified fuel, the toxic emissions as a fraction of VOC emissions is given by

^b Note that these coefficients apply to fuel properties that have been “standardized,” i.e., centered on their means and scaled by their standard deviations, based on the fuel-property matrix used to develop the models. To properly apply the models, this process must be applied for the specific fuels under consideration. For more information on this technique, please see the EPAct analysis report.

$$\text{Toxic Fraction} = f_{\text{toxic}} = \frac{e^{X\beta_{\text{toxic}}}}{e^{X\alpha_{\text{NMOG}}} - e^{X\theta_{\text{ethane}}}} \quad \text{Equation 13}$$

For these compounds, the calculation shown in Equation 13 is applied in the GeneralFuelRatioExpression table. Table 28 and Table 29 show coefficients for statistical models for ethanol and the five toxics representing “cold start” and “hot-running” emissions, respectively.

At this point, two important aspects of the EPA Act Phase 3 program must be noted. As resources available for the project limited the number of tests for which hydrocarbons could be speciated, some models were developed using smaller subsets of data representing fewer vehicles and fuels and are thus simpler in structure, including only the four linear terms ethanol, aromatics, T50 and T90, and no second-order terms. For simplicity, the smaller set of vehicles and fuels is termed the “reduced” design, in contrast to the “full” design. In addition, it is necessary to note that the fuel terms for models fit to the “reduced” design are standardized differently than those fit under the “full” design. The fuel property statistics for the reduced design are presented below in Table 27.

Coefficients for start emissions are presented in Table 30, as start emissions for four compounds were measured on the “full design”, with two compounds measured on the “reduced design.” However, as all models representing running emissions were developed using the reduced design, representing 5 vehicles measured on 11 fuels, these models are presented separately in Table 31.

In addition, because VOC are calculated as non-methane organic gases (NMOG) minus ethane (H_3CCH_3), it was necessary to develop analogous models for both NMOG and ethane. Coefficients for these two models are shown in Table 30 and Table 31 for start and running emissions, respectively. Models for these two compounds were calculated in the same manner as those for the toxic compounds. Note that models for both start and running ethane were developed using the reduced design, as with some of the toxics models.

In calculating toxic fractions, we elected to use models for NMOG and ethane fit using study designs and datasets similar to those for the toxic compounds. That is to say, if the toxic model was fit with the reduced design, we combined it with the NMOG and ethane models also fit with the reduced design. We followed this approach to prevent the calculation and propagation of artifacts in the estimated fractions resulting from differing levels of information and complexity in the numerator and denominator in Equation 13. In this context we considered it important to apply “information parity” to the toxic model in the numerator and the NMOG model in the denominator, as the vast majority of VOC mass is represented by NMOG, with ethane comprising only a small fraction.

Table 27. Means and Standard deviations for Fuel Properties, based on the Fuel Matrix in the EPAct Phase-3 Project.

Model Term	Full Design ¹		Reduced Design ²	
	Mean	Standard Deviation	Mean	Standard Deviation
Ethanol (%)	10.3137	7.87956	10.3137	7.87956
Aromatics (%)	25.6296	10.0154	25.6296	10.0154
RVP (psi)	8.5178	1.61137		
T50 (°F)	190.611	28.5791	190.611	28.5791
T90 (°F)	320.533	19.4801	320.533	19.4801
etOH × etOH	0.962963	0.802769		
T50 × T50	0.962963	0.739766		
etOH × Arom	-0.03674	0.978461		
etOH × RVP	-0.099235	0.999615		
etOH × T50	-0.541342	0.769153		
etOH × T90	0.0163277	0.972825		

¹ Applies to models fit with data from 13-15 vehicles measured on 27 fuels.

² Applies to models fit with data from five vehicles measured on 11 fuels.

Table 28. Models representing “Cold-start” Emissions for Selected Air Toxics.

Model term	Compound					
	Acetaldehyde ¹	Formaldehyde ¹	Acrolein ¹	Ethanol ¹	Benzene ²	1,3-Butadiene ²
Intercept	-5.2323	-5.9771	-7.9338	-4.9080	-4.1029	-5.8371
etOH	0.81449	0.2299	0.2476	1.4627	-0.00468	-0.01729
Arom	0.03483	0.02822	0.1122		0.4056	0.02673
RVP	-0.04170	-0.04718	-0.06450	-0.06054		
T50	0.08670	0.1672	0.1880	0.07029	0.04242	0.1247
T90	0.03801	0.1302	0.2489	-0.09923	0.01133	0.1004
etOH × etOH	-0.1669		-0.08310	-0.4970		
T50 × T50	0.06665	0.05262		0.1108		
etOH × Arom	0.01840	0.01651				
etOH × RVP	0.02194					
etOH × T50		-0.01627	-0.1186			
etOH × T90		0.02004	0.04617			
T50 × T90	0.03959	0.03489	0.05986			
Variance (s^2_ϵ)	0.2034	0.4765	0.4661	0.7013	0.4614	0.3281

¹ Models fit under the full design, including 15 vehicles measured on 27 fuels. See Table 27.

² Models fit under the reduced design, including 15 vehicles measured on 11 fuels. Note that these models do not include a linear term for RVP, and do not include any 2nd-order terms.

Table 29. Models representing “Hot-Running” Emissions for Selected Air Toxics¹.

Model term	Acetaldehyde	Formaldehyde	Acrolein	Ethanol	Benzene	1,3-Butadiene
Intercept	-9.4189	-8.6574	MODEL	-9.3072	MODEL	MODEL
etOH	0.1520	0.08456		0.9233		
Arom	0.07991	0.01575		-0.3772		
T50	-0.02997	0.01863		-0.01910		
T90	-0.07836	-0.08138		-0.3017		
Variance (s^2_e)	0.4379	0.4583		1.4596		

¹ Models fit using data from 5 vehicles measured on 11 fuels.

Table 30. NMOG and Ethane (Bag 1):

Models representing “Cold-start” Emissions under Full and Reduced Designs.

Model term	Full Design ¹	Reduced Design ²	
	NMOG	NMOG ³	Ethane ⁴
Intercept	-0.95209	-0.8943	-4.3079
etOH	0.08019	0.1040	0.1204
Arom	0.08782	0.09435	-0.1728
RVP	-0.04224		
T50	0.1345	0.1527	0.2169
T90		0.02127	0.09531
etOH × etOH	0.04432		
T50 × T50	0.07579		
etOH × Arom	0.01693		
etOH × RVP			
etOH × T50	0.04653		
etOH × T90	-0.95209		
Variance (s^2_e)	0.2012	0.1982	0.6377

¹ Represents 15 vehicles measured on 27 fuels; this model is used with the “full-design” models for Acetaldehyde, Formaldehyde, Acrolein and Ethanol, shown in Table 28 above.
² Represents 15 vehicles measured on 11 fuels.
³ This model used with models for Benzene and 1,3-butadiene shown in Table 28 above.
⁴ This model used with all models shown in Table 28; note that ethane was measured only under the reduced design.

**Table 31. NMOG and Ethane (Bag 2):
Models representing “Hot-Running” Emissions under the Reduced Design**

Model Term	Model ¹	
	NMOG	Ethane
Intercept	-4.7775	-7.7241
etOH	0.01778	0.07345
Arom	0.03320	-0.1260
T50	0.04258	0.1815
T90	0.09051	0.1322
Variance (s^2_{ϵ})	1.2431	2.8243
¹ These models used with all models listed in Table 29.		

2.2.1.3 Estimating Simple Fractions for Running Emissions

In Table 29 above, note that models representing running emissions are not available for three compounds: acrolein, benzene and 1,3-butadiene. For these compounds, the relevant subsets of data were inadequate to allow model fitting. Therefore, for these compounds, running emissions were represented as “simple” (constant) fractions of VOC, with values derived from the available data.

Thus, for acrolein, benzene and 1,3-butadiene, the values of the fractions were 0.00077, 0.047 and 0.0, respectively. These values were derived as “ratios of means” (ROM), in which the toxic and VOC values were averaged first by vehicle and then across vehicles, as described below. The ROM approach is generally preferred as it provides an unbiased estimator of the true fraction as the sample size increases¹⁹.

For benzene, results were available for four vehicles, differing widely in their benzene and VOC levels, and also in numbers of available measurements, as shown in Table 32. The averaging was performed in two steps so that the vehicle(s) with the greatest numbers of measurements would not dominate the overall mean. In the first step, the benzene and VOC values were averaged for each vehicle. In the second step, the four vehicle means were averaged to give an overall mean. Finally, the overall mean for benzene was divided by that for VOC to give a simple ratio estimator for benzene as a fraction of VOC.

Table 32. Benzene (Running):

Derivation of a Ratio-of-Means Estimator for Benzene as a Fraction of VOC.

Vehicle	<i>n</i>	Benzene (mg)	VOC (mg)	Ratio of means (ROM) ¹
Corolla	2	0.053752	2.2694	
F150	10	2.2241	28.427	
Impala	3	0.10825	10.670	
Silverado	4	0.29381	16.216	

All vehicles	4	0.669971	14.396	0.0465
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¹ This value is a simple average of the means for all four vehicles, as listed above.

The VOC fraction for acrolein was derived similarly (Table 33). For this compound results were available for five vehicles. Values for acrolein are considerably lower than for benzene, so results are expressed in μg , rather than mg. The resulting fraction is two orders of magnitude lower than that for benzene.

Table 33. Acrolein (Bag 2):**Derivation of a Ratio-of-Means Estimator for Acrolein as a Fraction of VOC.**

Vehicle	<i>n</i>	Acrolein (μg)	VOC (μg)	Ratio of means (ROM)
Civic	3	5.4190	3,038.9	
Corolla	5	2.8934	2,929.6	
F150	5	8.3558	24,321	
Impala	6	8.0180	10,408	
Silverado	10	19.662	17,192	

All vehicles	5	8.8696 ¹	11,578	0.0007661
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¹ This value is a simple average of the means for all five vehicles, as listed above.

For 1,3-butadiene in hot-running operation, measurements were extremely low; in fact, we considered the dataset so heavily affected by “left-censoring” that we did not consider it adequate for either model fitting or development of ratio estimators. Accordingly, for modeling purposes, we have adopted an assumption that this compound is not emitted during hot-running operation, i.e., the ROM estimator is 0.0.

2.2.1.4 Post-Model Adjustments

For two compounds, benzene and 1,3-butadiene, additional refinements were applied to supplement the study design of the EPAct fuel set. These adjustments are applied to both start and running emissions.

For benzene, the issue is that the fuel matrix included aromatics generally, but not benzene specifically. As we considered it inadequate to model benzene in exhaust without explicitly accounting for benzene levels in fuel, we developed a “post-model” refinement using data external to the EPAct program. In this case the source was a program conducted in support of the 2007 MSAT2 rule. This program performed measurements on nine Tier-2 certified vehicles on fuels with benzene levels ranging from 0.6 to 1.1 percent by weight.^{20,21} With benzene represented as a fraction of VOC (as in Equation 13) denoted as f_{benzene} , a value modified to account for benzene levels in different fuels (f_{benzene}^*) is calculated as shown in Equation 14 where x_{benzene} is the benzene level for the fuel modeled (weight percent), A is the mean benzene level in the EPAct exhaust program fuel set (0.66 weight percent), and B is an empirical coefficient, taking a value of 0.24.

$$f_{\text{benzene}}^* = [(x_{\text{benzene}} - A) \cdot B \cdot f_{\text{benzene}}] + f_{\text{benzene}} \quad \text{Equation 14}$$

Similarly, given the importance of olefins to estimation of emissions for 1,3-butadiene, and that the EPAct exhaust program study design did not incorporate olefins as a factor, we considered it appropriate to develop a post-model adjustment explicitly accounting for olefin level. This adjustment was derived by varying olefin levels in the Complex Model1 and fitting a polynomial trend to the results.²² Starting with an unadjusted toxic fraction for 1,3-butadiene (f_{buta}), the modified fraction f_{buta}^* is calculated using Equation 15, in which x_{olefin} is the olefin

level, and A , B , C and D are coefficients, taking values of 0.000008, 0.0002, 0.0069 and 0.008823, respectively.

$$f_{\text{buta}}^* = f_{\text{buta}} \left(\frac{Ax_{\text{olefin}}^2 + Bx_{\text{olefin}} + C}{D} \right) \quad \text{Equation 15}$$

2.2.2 Gaseous Hydrocarbons

2.2.2.1 Vehicles operating on Fuel blends containing 0-20% Ethanol

2.2.2.1.1 Additional Air Toxics

For fuel blends with 0%, 10% and 15% ethanol, composite speciation profiles developed from the results of EPAAct (Phase 1) were used to develop toxic fractions for the hazardous air toxics included in Table 34.^c These profiles were based on averaging results of tests from 3 vehicles.^{23,24} Toxic fractions for E10 are used for all gasolines containing ethanol levels of 5 vol.% or greater. For fuel blends containing 20% ethanol fractions were developed using a composite speciation profile developed using results from the EPAAct (Phase 3) program. The fractions are also presented in Table 34. For blends containing MTBE, no data were available for Tier 2 vehicles; thus the toxic to VOC ratios for Tier 1 and earlier vehicles were used (See Table 14, page 17). The values shown in the Table 34 are stored in the database table minorHAPRatio (see Table 16, page 19).

^c Phase 1 testing was done using fuels more representative of in-use fuels, in contrast to the orthogonal matrix used for EPAAct Phase 3.

Table 34. Toxic fractions for Selected Compound, Representing Model years 2004 and Later.

Pollutant (pollutantID) ¹	Fuel Blends (Gasoline & “Gasohol”)			
	0% (E0)	10% (E10)**	15% (E15)	20% (E20)
2,2,4-Trimethylpentane (40)	0.03188	0.01227	0.02199	0.004625
Ethyl Benzene (41)	0.01683	0.01660	0.01568	0.022199
Hexane (42)	0.002790	0.02911	0.0110	0.02497
Propionaldehyde (43)	0.00122	0.00054	0.0005984	0.0006607
Styrene (44)	0.00085	0.00083	0.004588	0.004096
Toluene (45)	0.07542	0.07440	0.0727	0.09646
Xylene(s) (46)	0.06127	0.06047	0.06902	0.09302

¹ For fuels containing 0-20% ethanol, fractions for ethanol, benzene, acetaldehyde, formaldehyde, 1,3-butadiene, and acrolein were estimated using methods described in 2.2.1.2 - 2.2.1.4.

**Values also applied for fuels containing 5% and 8% ethanol, (E5 and E8).

2.2.2.2 Vehicles operating on Fuel blends containing 70-100% Ethanol

2.2.2.2.1 Major Hazardous Air Pollutants (HAPs)

For major HAPs, instead of deriving toxic fractions, adjustment factors were developed based on the analysis of EPA Act (phase 3) program, National Renewable Energy Laboratory (NREL) E40²⁵, Coordinating Research Council (CRC) E-80²⁶, and PM Speciation Program²⁷. All programs measured emissions from LA92 test cycle on both E10 and E85, except CRC E-80 which tested E6 and E85. Only the vehicles tested on both E10 (E6) and E85 were included in the analysis. The number of vehicles from each program is summarized in Table 35.

Table 35. Number of vehicles included in the analysis of major HAPs

Test Program	Number of Vehicles
EPA Act (phase 3)	3
NREL E40	9
CRC E-80	7
PM Speciation	2

Consistent emission trends were observed across datasets and thus, all available datasets were pooled to examine the effect of E85 on emissions compared to E10. First, the test of significance of differences between E10 and E85 was performed using Student’s paired t-tests. Next, when there was a statistically significant difference in emissions between E10 and E85, the adjustment factors were calculated using Equation 16. The adjustment factor was set to zero when the differences in emissions were not statistically different (i.e., acrolein).

$$E85 \text{ adjustment factor} = \frac{\frac{Toxics_{E85}}{VOC_{E85}}}{\frac{Toxics_{E10}}{VOC_{E10}}} \quad \text{Equation 16}$$

The resulting adjustment factors are shown in Table 36, and are stored in the database table, “GeneralFuelRatioExpression”, for fuelTypeID = 5.

Table 36. E70/E85 adjustment factors for major HAPs

Pollutant (pollutantID)	Adjustment Factor for E70/E85
Benzene (20)	0.6672
Ethanol (21)	7.587
1,3-butadiene (24)	0.2167
Formaldehyde (25)	1.572
Acetaldehyde (26)	7.126
Acrolein (27)	0

2.2.2.2.2 Additional Air Toxics

Toxic fractions for additional air toxics (pollutantID from 40-46) for model year 2001 and later are identical to the fractions for model year 2000 and earlier, as shown in Table 34.

2.2.3 Polycyclic Aromatic Hydrocarbons (PAH)

2.2.3.1 Vehicles operating on Fuel blends containing 0-20% Ethanol

In the absence of additional data, the fractions for more recently manufactured vehicles were assumed to be similar to those for vehicles employing older technologies. See Table 20, page 23.

2.2.3.2 Vehicles operating on Fuel blends containing 70-85% Ethanol (E70/E85)

Limited emissions data exist for PAH emissions from vehicles running on E85. Thus, toxic fractions for PAH relative to OC_{2.5} VOC were estimated by multiplying the fractions for E0 fuels (Table 20) by the fraction of gasoline in E85 fuel. We assumed that annual average ethanol content of E85 is 74%. Thus, E0 fractions were multiplied by 0.26. This approach assumes that no PAH emissions result from ethanol combustion. The resulting fractions presented in Table 37

Table 37. Toxic Fractions for PAH Species for Vehicles running on E85 blends, by Phase and Process.

Species	pollutantID	CAS	Toxic fraction		
			Gaseous Phase	Particulate Phase	
				Start	Running
Naphthalene	23	91203	4.60E-02	4.37E-03	3.35E-03
Acenaphthylene	42	208968	4.03E-03	1.30E-03	9.97E-04
Acenaphthene	41	83329	8.87E-04	0.00E+00	0.00E+00
Fluorene	54	86737	1.80E-03	0.00E+00	0.00E+00
Anthracene	44	120127	7.44E-04	1.35E-03	1.03E-03
Phenanthrene	57	85018	4.77E-03	4.71E-03	3.61E-03
Fluoranthene	53	206440	1.24E-03	4.77E-03	3.65E-03
Pyrene	59	129000	1.42E-03	5.16E-03	3.95E-03
Benz(a)anthracene	45	56553	1.20E-04	1.24E-02	9.48E-03
Chrysene	50	218019	1.34E-04	1.05E-02	8.01E-03
Benzo(a)pyrene	46	50328	6.54E-06	3.10E-02	2.37E-02
Benzo(b)fluoranthene	47	205992	8.91E-05	1.51E-02	1.16E-02
Benzo(k)fluoranthene	49	207089	8.91E-05	1.51E-02	1.16E-02
Benzo(g,h,i)perylene	48	191242	0.00E+00	8.39E-02	6.42E-02
Indeno(1,2,3,c,d)pyrene	56	193395	0.00E+00	3.15E-02	2.41E-02
Dibenzo(a,h)anthracene	51	53703	0.00E+00	7.24E-04	5.55E-04

2.2.4 Metals

Since metal emissions can result from trace level contamination of fuel and engine oil, as well attrition from exhaust emission components, there is no way to estimate metal emissions for vehicles running on E85 or E70 fuel in the absence of data. Thus metal emission rates were assumed to remain unchanged from those applicable to vehicles with earlier fuel delivery and emissions control technologies (see Table 21, page 24).

2.2.5 Dioxins and Furans

2.2.5.1 Vehicles operating on Fuel blends containing 0-20% Ethanol

In the absence of additional data, the fractions for more recently manufactured vehicles were assumed to be similar to those for vehicles employing older technologies. See Table 24, page 26.

2.2.5.2 Vehicles operating on Fuel blends containing 70-85% Ethanol (E70/E85)

No emissions data exist for dioxin and furan emissions from vehicles running on E85 or E70. Thus dioxin emission factors for E85 and E70 were estimated by multiplying fractions for vehicles running on E0 fuels (Table 24) by the fraction of gasoline in the fuel, assuming no emission of dioxins or furans resulting from the combustion of ethanol. Resulting ratios are given in Table 38.

Table 38. Emission Factors for Dioxins and Furans, for Vehicles Operating on E85 Blends.

Congener	Emission rate (mg/mile)
2,3,7,8-Tetrachlorodibenzo-p-dioxin	2.15E-10
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	9.61E-11
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	1.01E-11
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	2.06E-11
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	1.28E-11
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	1.55E-11
Octachlorodibenzo-p-dioxin	3.67E-12
2,3,7,8-Tetrachlorodibenzofuran	7.19E-11
1,2,3,7,8-Pentachlorodibenzofuran	1.03E-11
2,3,4,7,8-Pentachlorodibenzofuran	7.55E-11
1,2,3,4,7,8-Hexachlorodibenzofuran	2.84E-11
1,2,3,6,7,8-Hexachlorodibenzofuran	3.02E-11
1,2,3,7,8,9-Hexachlorodibenzofuran	8.24E-12
2,3,4,6,7,8-Hexachlorodibenzofuran	3.52E-11
1,2,3,4,6,7,8-Heptachlorodibenzofuran	3.16E-11
1,2,3,4,7,8,9-Heptachlorodibenzofuran	1.01E-12
Octachlorodibenzofuran	1.07E-12

2.3 Heavy-Duty Diesel Vehicles: MY 2007 and Earlier

Toxic fractions and metal emission rates were developed for exhaust emissions from heavy-duty diesel vehicles and applied to all diesel vehicle categories. There are no separate emission ratios or factors for diesel engines running on biodiesel fuels or synthetic diesel fuels, due to very limited data.

The composition of hydrocarbons emissions for heavy-duty diesel engines lacking the advanced control technologies applied in more recently manufactured vehicles differ substantially. Thus, we developed one set of toxic fractions for pre-2007 diesel engines and another set for engines manufactured in 2007 and later.

2.3.1 Gaseous Hydrocarbons

To estimate toxic fractions for vehicles in this model-year group EPA relied on a database compiled for the Coordinating Research Council and the National Renewable Energy Laboratory (NREL) (CRC E-75).²⁸ This database was developed from a literature survey and compiled data collected in 13 different studies. The studies included were conducted in a number of different countries, included heavy-duty and light-duty engines, a variety of diesel and biodiesel fuels, and a number of different operating modes and cycles.

For 2,2,4-trimethylpentane, n-hexane, propionaldehyde, and toluene, toxic fractions were developed by Sierra Research. Their analysis of CRC E-75 data is described in detail in their technical report. Data from tests using non-conventional diesel fuel (Fischer-Tropsch, bioDiesel, ethanol-Diesel blends, emulsified fuel, European blends, and other obvious research fuels) were excluded, as were data from non-heavy duty engines. The fractions are provided in Table 39.

Toxic fractions for other compounds in Table 39 were developed by EPA from the E-75 database. We relied on data collected in the United States from heavy-duty diesel engines running on conventional diesel fuels, collected on test-cycles representative of real world operation. Some studies reported results on a distance-specific basis (g/mi) whereas others reported results on a brake-specific basis (g/hp-hr). For both subsets of data, we calculated mean emissions for each toxic and for VOC, and then calculated mean fractions for each reporting basis. We then calculated an overall mean fraction using the respective sample sizes to weight the two fractions. The resulting ratios are also provided in Table 39.

Table 39. Toxic Fractions for pre-2007 Diesel Engines.

Pollutant	Toxic fraction
1,3-Butadiene	0.002918
2,2,4-Trimethylpentane	0.001808
Acetaldehyde	0.035559
Acrolein	0.006622
Benzene	0.007835
Ethyl Benzene	0.002655
Formaldehyde	0.078225
n-Hexane	0.00197
Propionaldehyde	0.00468
Styrene	0.001312
Toluene	0.00433
Xylenes	0.003784

2.3.2 *Polycyclic Aromatic Hydrocarbons*

As with gasoline emissions, PAH mass emissions from diesel engines were apportioned into gaseous and particulate phases, using a single set of allocation factors for all temperature conditions. The partitioning factors for diesel PAHs were developed by Sierra Research²⁹ using estimates from EPA's SPECIATE 4.2 database³⁰ and information on compounds' physical and chemical properties. The allocations from SPECIATE were based on medium duty diesel engine data.³¹ The phase-partitioning factors are shown in Table 40. Compared to the partitioning for gasoline (Table 19, page 22 **Error! Bookmark not defined.**), the fraction of PAH in the particulate phase is higher for diesel emissions, which is consistent with the higher concentrations of particles in diesel exhaust.

Table 40. Phase-Partition Fractions for Emissions of Polyaromatic Hydrocarbons from Diesel Engines.

PAH species	Molar Mass (g/mol)	Phase Fraction	
		Gaseous	Particulate
Napthalene	128	1.0	0.0
Acenaphthylene	152	1.0	0.0
Acenaphthene	154	1.0	0.0
Fluorene	166	0.785	0.215
Anthracene	178	0.534	0.466
Phenanthrene	178	0.665	0.335
Fluoranthene	202	0.484	0.516
Pyrene	202	0.448	0.552
Benz(a)anthracene	228	0.277	0.723
Chrysene	228	0.177	0.823
Benzo(a)pyrene	252	0.0	1.0
Benzo(b)fluoranthene	252	0.0	1.0
Benzo(k)fluoranthene	252	0.0	1.0
Benzo(g,h,i)perylene	276	0.227	0.773
Indeno(1,2,3-cd)pyrene	276	0.0	1.0
Dibenzo(a,h)anthracene	278	0.0	1.0

Emissions of PAH in the gaseous and particulate phases were estimated as fractions of total VOC and Organic carbon emissions (OC_{2.5}), respectively. Toxic fractions were calculated using results from the E-75 database. For the particulate phase, a fraction was first calculated with respect to total PM_{2.5}, and then converted to a fraction of total OC_{2.5} using estimates of OC as a fraction of total PM_{2.5}. Note that the OC:PM fractions differed by emissions process, with separate fractions applied for start, running and extended-idle emissions.

In estimating fractions, we relied on data collected in the United States on heavy-duty diesel engines running on conventional diesel fuels, measured on test-cycles representative of real world operation. It should be noted that for some compounds, substantially more data was available than for others; thus the level of confidence in emission rates varies among individual compounds. For instance, while data from 66 tests were available for acenaphthene, data from only two tests were available for dibenz(a,h)anthracene. Table 41 shows fractions for PAH emissions relative to OC and VOC, by emissions process.

The PAH fractions for exhaust emissions are also applied to crankcase emissions. Because the PAH emissions are applied to the OC emissions, the total PM_{2.5} crankcase emissions in MOVES are more enriched with PAHs than tailpipe PM_{2.5} emissions, due to the large fraction OC/PM_{2.5} emissions in crankcase emissions. Research suggests that PM emissions from the crankcase are more enriched with PAHs than emissions from the exhaust.³²

Table 41. Toxic Fractions for PAH Species, by Phase and Process, for pre-2007 Heavy-Duty Diesel Engines.

Compound	Particulate Phase (OC _{2.5})			Gaseous Phase (VOC)
	Start	Extended Idle	Running (crankcase)	
Naphthalene	0.0	0.0	0.0	0.009046
Acenaphthylene	0.0	0.0	0.0	0.000501
Acenaphthene	0.0	0.0	0.0	0.000321
Fluorene	0.000280	0.000254	0.000849	0.000591
Anthracene	0.000163	0.000148	0.000494	0.000235
Phenanthrene	0.000644	0.000586	0.001956	0.001945
Fluoranthene	0.000624	0.000568	0.001896	0.000611
Pyrene	0.000902	0.000821	0.002740	0.000758
Benzo(a)anthracene	0.000323	0.000294	0.000981	0.000045
Chrysene	0.000204	0.000186	0.000620	0.000024
Benzo(a)pyrene	0.000121	0.000110	0.000369	0.0
Benzo(b)fluoranthene	0.000036	0.000033	0.000110	0.0
Benzo(k)fluoranthene	0.000005	0.000005	0.000015	0.0
Indeno(1,2,3-cd)pyrene	0.000009	0.000008	0.000028	0.0
Benzo(g,h,i)perylene	0.000006	0.000005	0.000018	0.0000276
Dibenz(a,h)anthracene	0.000005	0.000004	0.000015	0.0

2.3.3 Metals

Emission rates for selected metals representing pre-2007 heavy-duty diesel engines were based on data from the CRC E-75 program, with the exception of rates for mercury and arsenic. Emission rates for these metals were obtained from the same tunnel study used to supply the arsenic rates for gasoline vehicles (see Table 21, page 24). They do not vary with emission control technology. Table 42 provides metal emission factors for pre-2007 heavy duty engines.

Table 42. Emission Rates for Selected Metals, for pre-2007 Heavy-Duty Diesel Engines.

Pollutant	Emission Rate (g/mi)
Chromium III	5.6×10^{-6}
Chromium VI	1.2×10^{-6}
Manganese	8.0×10^{-6}
Nickel	1.4×10^{-5}
Mercury, Elemental Gaseous Phase	6.2×10^{-9}
Mercury, Reactive Gaseous Phase	3.2×10^{-9}
Mercury, Particulate Phase	1.6×10^{-9}
Arsenic	2.3×10^{-6}

2.3.4 Dioxins and Furans

To represent emissions of dioxins and furans from pre-2007 heavy-duty diesel engines, emissions rates for 17 congeners were calculated from the results of an EPA diesel dioxin/furan study of legacy engines³³. In this study, dioxin emissions from three heavy-duty engines were measured, manufactured in model year 1984 (GM 6.2 L), 1987 (Detroit Diesel 6V92) and 1993 (Cummins L10). The emission factors in mg/mi TEQ are shown in Table 43.

Table 43. Emission Rates for Dioxin/Furan Congeners, for pre-2007 Heavy-duty Diesel engines.

Congener	Emission Rate (mg/mi TEQ)
2,3,7,8-Tetrachlorodibenzo-p-dioxin (TCDD)	2.23×10^{-10}
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	0
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	0
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	1.03×10^{-11}
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	4.78×10^{-11}
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	4.18×10^{-11}
Octachlorodibenzo-p-dioxin	4.84×10^{-12}
2,3,7,8-Tetrachlorodibenzofuran	6.50×10^{-10}
1,2,3,7,8-Pentachlorodibenzofuran	4.16×10^{-11}
2,3,4,7,8-Pentachlorodibenzofuran	6.69×10^{-10}
1,2,3,4,7,8-Hexachlorodibenzofuran	8.02×10^{-11}
1,2,3,6,7,8-Hexachlorodibenzofuran	4.24×10^{-11}
1,2,3,7,8,9-Hexachlorodibenzofuran	0.0
2,3,4,6,7,8-Hexachlorodibenzofuran	3.03×10^{-11}
1,2,3,4,6,7,8-Heptachlorodibenzofuran	2.16×10^{-11}
1,2,3,4,7,8,9-Heptachlorodibenzofuran	0.0
Octachlorodibenzofuran	5.56×10^{-13}

2.4 Heavy-Duty Diesel Vehicles: MY 2007 and later

2.4.1 Gaseous Hydrocarbons

For heavy-duty diesel engines manufactured in 2007 and later, and light-duty diesel engines meeting Tier 2 emissions standards, advanced emission controls change the composition of

VOCs. For these engines, we relied on speciated emissions data from the Advanced Collaborative Emissions Study (ACES), directed by the Health Effects Institute and Coordinating Research Council, with participation from a range of government and private-sector sponsors.³⁴ In this study detailed emissions measurements were performed on four engines operated on low-sulfur diesel fuel over several test cycles. We made use of data from a 16-hour transient cycle. Toxic fractions calculated from the ACES data are provided in Table 44.

Table 44. Toxic Fractions for Heavy-duty Diesel Engines manufactured in 2007 and later.

Pollutant	Toxic fraction
1,3-Butadiene	0.00080
2,2,4-Trimethylpentane	0.00782
Acetaldehyde	0.06934
Acrolein	0.00999
Benzene	0.01291
Ethyl Benzene	0.00627
Formaldehyde	0.21744
N-Hexane	0.00541
Propionaldehyde	0.00314
Styrene	0.00000
Toluene	0.02999
Xylenes	0.03800

2.4.2 Polyaromatic Hydrocarbons

For heavy-duty diesels manufactured in 2007 and later, advanced emission controls reduce the total mass of PAH emitted and change the composition of these compounds. For these engines, we relied on speciated emissions data from the ACES study. Toxic fractions applicable to these engines are shown in Table 45, in which the fractions are differentiated by phase but not by emissions process. For the particulate phase, a single fraction is provided for all processes (similar to HC) because the OC/PM fraction in MOVES for 2007+ diesel is a single fraction for all emission processes. The OC/PM fraction is derived from measurements made on a 16-hour drive cycle that composes multiple driving modes as documented in the MOVES2014 TOG and PM Speciation Report.

Table 45. Toxic Fractions for Polyaromatic Compounds, by Phase, for Heavy-duty Diesel Engines manufactured in 2007 and later.

Compound	Particulate Phase (OC _{2.5})	Gaseous Phase (VOC)
Naphthalene	0	0.0163278
Acenaphthylene	0	0.0000853
Acenaphthene	0	0.0000526
Fluorene	0.0002409	0.0001963
Anthracene	0.0001187	0.0000304
Phenanthrene	0.0019187	0.0008507
Fluoranthene	0.0002181	0.0000457
Pyrene	0.0002091	0.0000379
Benzo(a)anthracene	0.0000036	0.0000003
Chrysene	0.0000112	0.0000005
Benzo(a)pyrene	0.0000148	0
Benzo(b)fluoranthene	0.0000063	0
Benzo(k)fluoranthene	0.0000063	0
Indeno(1,2,3-cd)pyrene	0.0000022	0
Benzo(ghi)perylene	0.0000009	0.0000002
Dibenz(a,h)anthracene	0.0000045	0

2.4.3 Metals

Emissions rates for selected metals representing heavy-duty diesel engines manufactured since 2007 were developed from data from the ACES program, with the exception of rates for mercury and arsenic. Rates for these two metals are identical to those used for gasoline engines (Table 21, page 24). Rates are presented in Table 46.

Table 46. Emission Rates for Metals, for Heavy-Duty Diesel Engines manufactured in 2007 and Later.

Pollutant	Emission Rate (g/mi)
Chromium III	1.6×10^{-6}
Chromium VI	3.4×10^{-7}
Manganese	5.5×10^{-7}
Nickel	6.5×10^{-7}
Mercury, Elemental Gaseous Phase	6.2×10^{-9}
Mercury, Reactive Gaseous Phase	3.2×10^{-9}
Mercury, Particulate Phase	1.6×10^{-9}
Arsenic	2.3×10^{-6}

2.4.4 Dioxins and Furans

The data used to calculate the emission rates for engines manufactured in 2007 and later were obtained from the EPA diesel dioxin study of 2007 and later engines.³⁵ The results represent measurements of transient tests conducted on a MY2008 Cummins ISB over 48 tests on the FTP cycle in a 1:23 cold/hot start ratio, combined with several emission-control technologies. To represent emissions from engines manufactured between 2007-2009, the results for the diesel oxidation catalyst plus catalyzed diesel particulate filter were used. For engines manufactured in 2010 and later, the results for the diesel oxidation catalyst plus catalyzed diesel particulate filter coupled with flow through copper zeolite selective catalytic reduction and urea and ammonia slip catalyst were used. Rates are presented in Table 47.

Table 47. Emission Rates for Dioxins and Furans, for Heavy-duty Diesel Engines manufactured in 2007 and later

Congener	2007 - 2009	2010 and later
2,3,7,8-Tetrachlorodibenzo-p-dioxin (TCDD)	0.0	0
1,2,3,7,8-Pentachlorodibenzo-p-Dioxin	0.0	0
1,2,3,4,7,8-Hexachlorodibenzo-p-Dioxin	0.0	0
1,2,3,6,7,8-Hexachlorodibenzo-p-Dioxin	0.0	0
1,2,3,7,8,9-Hexachlorodibenzo-p-Dioxin	4.11×10^{-12}	0
1,2,3,4,6,7,8-Heptachlorodibenzo-p-Dioxin	2.58×10^{-12}	1.05×10^{-11}
Octachlorodibenzo-p-dioxin	2.79×10^{-13}	2.09×10^{-12}
2,3,7,8-Tetrachlorodibenzofuran	0.0	5.09×10^{-12}
1,2,3,7,8-Pentachlorodibenzofuran	0.0	3.21×10^{-12}
2,3,4,7,8-Pentachlorodibenzofuran	1.89×10^{-11}	9.73×10^{-11}
1,2,3,4,7,8-Hexachlorodibenzofuran	0.0	2.20×10^{-11}
1,2,3,6,7,8-Hexachlorodibenzofuran	0.0	2.43×10^{-11}
1,2,3,7,8,9-Hexachlorodibenzofuran	0.0	0
2,3,4,6,7,8-Hexachlorodibenzofuran	0.0	1.80×10^{-11}
1,2,3,4,6,7,8-Heptachlorodibenzofuran	3.00×10^{-12}	9.94×10^{-12}
1,2,3,4,7,8,9-Heptachlorodibenzofuran	0.0	5.81×10^{-13}
Octachlorodibenzofuran	2.12×10^{-13}	$\times 10^{-13}$

2.5 Light-duty Diesel and Auxiliary Power Units

Since extended idle emissions associated with auxiliary power units (APUs) are not subject to 2007 standards, toxic to VOC ratios for pre-2007 diesel engines were used for them³⁶. Since light-duty diesels comprise a very small portion of the fleet, the heavy-duty ratios were applied to light-duty diesel vehicle classes to streamline modeling.

2.6 Compressed Natural Gas Emissions

Currently, MOVES2014 only models compressed natural gas (CNG) fueled transit buses. For simplification, all CNG-powered light-duty and heavy-duty vehicles are assumed to be fueled by gasoline or diesel. This section describes the development of toxic emission rates applied to CNG transit buses.

2.6.1 Gaseous Hydrocarbons

We used hydrocarbon speciation measurements from the testing by the California Air Resources Board³⁷ (Ayala et al. 2003) using measurements from the 2000 MY Detroit Diesel Series 50G engine with and without an oxidation catalyst collected on the CBD cycle. As discussed in the MOVES2014 heavy-duty report, we used the uncontrolled tests to represent speciation from pre-2002 CNG transit buses, and the oxidation catalyst tests to represent 2002 and later buses. We also used the Central Business District (CBD) cycle to be consistent with the criteria pollutant measurements.

The toxic fractions derived from this set of measurements are displayed in Table 48. The total VOC emissions rates are reduced by 70% from pre-2002 levels and the 2002-2006 model year groups in MOVES. As shown in Table 48, formaldehyde emissions are preferentially reduced by the oxidation catalyst. Formaldehyde contributes to over 50% of the VOC emissions for the uncontrolled CNG bus, but only 16.2% of the VOC emissions for the CNG bus equipped with an oxidation catalyst. The MOVES toxics not measured in this study are assumed to be negligible, and are modeled as 0.

Table 48. Toxic Fractions for CNG Transit Buses.

	No control (pre-2002)	With oxidation catalyst (2002+)
1,3 Butadiene	2.34E-04	0
Benzene	1.35E-03	2.53E-03
Toluene	6.91E-04	7.86E-03
Ethylbenzene	8.41E-05	1.31E-03
Xylenes	8.23E-04	6.34E-03
Formaldehyde	0.517	0.162
Acetaldehyde	0.0305	0.138
Acrolein	2.35E-03	0
Propionaldehyde	0.0153	0

2.6.2 Polycyclic Aromatic Hydrocarbons

The PAH toxic fractions for compressed natural gas are derived from tests on a MY2000 DDC Series 50G engine on a New Flyer CNG transit bus tested by the California Air Resources Board.³⁸ Emissions were measured in two stages (the bus was re-tested after 3 months of service

in the Los Angeles County Metropolitan Transit Authority. The PAH emissions were measured in the semi-volatile phase using PUF-XAD, and measured in the particulate phase on Teflon-coated glass fiber filters. VOC emissions are derived from the NMHC and speciated hydrocarbon emissions. The OC emissions rates were provided to EPA by CARB. We estimated the volatile PAH emissions by calculating PAH/VOC fractions from the PUF-XAD measurements, and particle-phase PAH/OC fractions using the filter-based measurements for both stages of the study. For use in MOVES, we averaged the ratios estimated from both stages of the testing. The average ratios are displayed in Table 49.

Table 49. PAH Ratios to volatile organic carbon (volatile PAHs), and to organic carbon (particle-phase).

Compound	VOC ratio	OC ratio
Naphthalene	9.554E-06	2.114E-05
Acenaphthylene	4.230E-06	ND
Acenaphthene	1.243E-06	1.886E-05
Fluorene	2.986E-06	3.301E-05
Anthracene	1.164E-06	1.644E-06
Phenanthrene	8.356E-06	2.043E-05
Fluoranthene	1.936E-06	2.874E-05
Pyrene	3.743E-06	5.350E-05
Benz(a)anthracene	1.682E-07	9.390E-06
Chrysene/triphenylene	2.441E-07	1.911E-05
Benzo(a)pyrene	ND	ND
Benzo(b)fluoranthene	ND	ND
Benzo(k)fluoranthene	ND	ND
Indeno(1,2,3-cd)pyrene	ND	ND
Benzo(g,h,i)perylene	ND	5.502E-06
Dibenz(a,h)anthracene	ND	ND

ND = not detected, fractions set to 0.

2.6.3 Metals

We used the chromium and nickel emission rates reported from the uncontrolled 2000 MY DDC Series 50G³⁹. We used the uncontrolled bus to be consistent with the PM_{2.5} speciation profile and because this was the only bus in the study that detected both pollutants. The chromium emissions were not significantly different between the uncontrolled and controlled DDC engine. The isotope split of chromium is based on the same assumptions used for gasoline¹².

The other metal emission rates produced by MOVES were not available in the published literature. As such, we used the same g/mile emission rates as gasoline.

Table 50. Metal emission rates and sources used for CNG Transit buses in MOVES.

Pollutant	Emission Rate (g/mi)	Source
Chromium 6+	1.26E-08	Okamoto et al. (2006)
Chromium 3+	5.74E-08	Okamoto et al. (2006)
Manganese	1.33E-06	Same as gasoline
Nickel	1.00E-08	Okamoto et al. (2006)
Elemental Gas Phase Hg	1.10E-07	Same as gasoline
Reactive Gas Phase Hg	9.90E-09	Same as gasoline
Particulate Hg	4.00E-10	Same as gasoline
Arsenic	2.30E-06	Same as gasoline

2.6.4 Dioxins and Furans

No published dioxin and furan emission rates for CNG vehicles were available to the US EPA. As such, we are using the dioxin emission rates for gasoline reported in Table 24 (page 7).

3 Evaporative Emissions

3.1 Light-Duty Vehicles (Gasoline-powered): MY???? <2.1>

As with exhaust emissions, emissions of toxics emitted through evaporation of unburned fuel as also estimated as fractions of total (evaporative?) VOC. Again, fractions for some compounds are estimated as complex fractions based on fuel properties such as oxygenate content and vapor pressure. For other compounds, simple fractions are estimated. For the compounds modeled, fraction types and data sources are summarized in Table 51.

3.1.1 Non-permeation processes

Algorithms used to generate complex fractions were adapted from those used in MOBILE6.2.⁴⁰ However, as the conceptual basis for modeling evaporative emissions has changed in MOVES, the equations are applied to the emission processes considered most closely analogous. Thus, algorithms for hot soak in MOBILE6.2 are used for vapor venting and refueling vapor loss, and algorithms for running loss are used for fuel leaks and refueling spillage loss. The equations are applied for fuels containing up to 10% ethanol, and are presented in Table 52.

Simple Fractions for other air toxics in evaporative non-permeation emissions were obtained from profiles developed for EPA by Environ Corporation, using data from the Auto/Oil program conducted in the early 1990's.⁴¹ The fractions for these compounds are the same for all pollutant processes (except permeation) and are presented in Table 53.

Ratios for naphthalene and ethanol are derived from <source?>, and are also shown in Table 53.

The ratios for 10% ethanol are used for all fuels with greater than or equal to 5% ethanol and less than 12%.

Conventional gasoline ratios are also used for MTBE oxygenated gasoline.

For vehicles operating on fuels containing 15% ethanol (E15), no data describing evaporative emissions are available. For the vapor-venting and spillage emission processes, emission rates calculated from E15 and E10 fuel speciation data from the EPA Act Program were used to adjust the E10 evaporative emissions speciation.⁴² Resulting toxic fractions are provided in Table 53.

For vehicles containing 20% ethanol, toxic fractions were developed for fuel speciation profiles developed from data collected in the EPA Act program. Average fractions by weight were calculated as a composite of data from the seven E20 blends included in the fuel matrix. Resulting fractions are shown in Table 53.

For vehicles operating on fuels containing high levels of ethanol, ranging from 70 to 100%, the toxic fractions were developed based on the two-day diurnal evaporative emissions test from four 2007 model year FFVs from CRC E-80 program²⁶. Following the typical speciation profile procedures, the fraction of each compound in a test was first calculated by dividing its emission factors (EFs) by the sum of all EFs for that test, and the percentages for a given compound were then averaged across all tests to form the composite profile. The resulting fractions are presented in Table 53.

Table 51. Data Sources and Estimation Methods Used in Estimation of Toxic Fractions for Evaporative Hydrocarbons.

Compound	Process	Fraction Type	Basis for Estimation
Benzene	Vapor venting/refueling (vapor)	complex	Adapted from MOBILE6.2
	Fuel leaks/spillage	complex	Adapted from MOBILE6.2
MTBE	Vapor venting/refueling (vapor)	complex	Adapted from MOBILE6.2
	Fuel leaks/spillage	complex	Adapted from MOBILE6.2
2,2,4-trimethylpentane	All (except permeation)	simple	Speciation profile
Ethylbenzene	All (except permeation)	simple	Speciation profile
N-Hexane	All (except permeation)	simple	Speciation profile
Propionaldehyde	All (except permeation)	simple	Speciation profile
Toluene	All (except permeation)	simple	Speciation profile
Xylenes	All (except permeation)	simple	Speciation profile
Naphthalene		simple	
Ethanol		simple	

Table 52. Complex fractions for Evaporative Emissions of Two Compounds.

Pollutant	Process	Equation for Toxic Fraction
Benzene	Vapor venting/Refueling (vapor)	$(-0.03420 * OXY - 0.080274 * RVP + 1.4448) * BNZ / 100$
	Fuel Leaks/Spillage	$(-0.03420 * OXY - 0.080274 * RVP + 1.4448) * BNZ / 100$
MTBE	Vapor Venting/Refueling (vapor)	$(24.205 - 1.746 * RVP) * MTBE / 1000$
	Fuel Leaks/Spillage	$(17.8538 - 1.6622 * RVP) * MTBE / 1000$
OXY = oxygen content (wt%) RVP = Reid Vapor Pressure (psi) BNZ = benzene content (vol.%) MTBE = methyl-tertiary-butyl ether content (vol.%).		

Table 53. Toxic Fractions for Evaporative Emissions, for Vapor-venting and Refueling-spillage Processes.

Pollutant	Ethanol Level				
	0.0% (E0)	10% (E10)	15% (E15)	20% (E20)	70-100%
Ethanol	0.00000	0.11896	0.1935	0.2227	0.61042
Naphthalene	0.00040	0.00040	0.0000	?	0
2,2,4-Trimethylpentane	0.01984	0.03354	0.05313	0.0430	0.00830
Ethyl Benzene	0.02521	0.01721	0.01662	0.0155	0.00124
N-Hexane	0.02217	0.02536	0.007478	0.0186	0.01276
Toluene	0.09643	0.14336	0.1406	0.0874	0.01608
Xylene ^a	0.07999	0.06423	0.05735	0.0711	0.00733
Benzene			0.02758	0.0073	0.00664

3.1.2 Permeation

The composition of hydrocarbons emitted through permeation differs substantially from that of hydrocarbons emitted through other processes. Work to better characterize these permeation emissions was recently conducted by Southwest Research Institute for EPA and the Coordinating Research Council.⁴³ Data from 3-day diurnal tests on vehicles meeting Tier 1 and near-zero evaporative emission standards were used. Fractions representing emissions of toxic compounds relative to total VOC were estimated for gasoline fuels containing 0-10% ethanol by averaging data from fuels with varying vapor pressures. Fractions are presented in Table 54, for all compounds except benzene and naphthalene.

For benzene, the diurnal emissions equation from MOBILE6.2 was used to calculate the permeation fraction $f_{benz,permeation}$, since it accounts for changes in oxygenate, vapor pressure and fuel benzene levels, as shown in Equation 17.⁴⁴ However, a study of permeation emissions

suggests that the fraction of benzene from permeation is about 1.77 times higher than the ratio associated with evaporation.⁴⁵ Thus the diurnal emissions algorithm was multiplied by 1.77.

$$f_{\text{benz,permeation}} = 1.77[(-0.02895 \text{ OXY} - 0.080274 \text{ RVP} + 1.3758) \text{ benz} / 100] \quad \text{Equation 17}$$

In the absence of data on permeation emissions for MTBE, a complex fraction $f_{\text{MTBE,permeation}}$ is calculated using the resting-loss algorithm from MOBILE6.2 (Equation 18).

$$f_{\text{MTBE,permeation}} = (22.198 - 1.746 \text{ RVP}) \text{ MTBE} / 1,000 \quad \text{Equation 18}$$

To estimate toxic fractions for vehicles operating on fuels containing 15% ethanol, the fractions for E10 and E20 fuels were linearly interpolated for ethanol levels of 15%. The fractions for the E10 and E20 fuels were derived from the CRC E-77-2b and CRC E-77-2c test programs.^{46,47} Toxic fractions are shown in Table 54.

For vehicles operating on fuels containing 20% ethanol, fractions were developed using data from the CRC E-77-2c test program.⁴⁸ Fractions are presented in Table 54.

Table 54. Toxic Fractions Representing Permeation Emissions as Components of Total VOC Emissions, by Ethanol Level (Source: CRC E-77-2b).

Pollutant	Ethanol Level				
	0.0% (E0)	10% (E10)	15% (E15)	20% (E20)	70-100%
2,2,4-Trimethylpentane	0.036	0.024	0.0172	0.0107	0.00830 ¹
Ethylbenzene	0.003	0.001	0.0017	0.0019	0.00124 ¹
N-Hexane	0.050	0.065	0.0472	0.0308	0.01276 ¹
Toluene	0.110	0.101	0.0666	0.0354	0.01608 ¹
Xylene(s)	0.016	0.011	0.0127	0.0140	0.00733 ¹
Ethanol	0.000	0.202	0.2694	0.3296	0.61042 ¹
Naphthalene ¹			0.0000		0 ¹
Benzene			0.0236	0.0244	0.00664 ¹

¹ Identical to fractions for the vapor-venting process, based on CRC E-80 program (Table 53).

For ethanol levels less than 10% and less, the toxic fraction for non-permeation evaporative emissions was also applied to permeation.

3.2 Diesel Vehicles (heavy-duty, light duty?)

For diesel-fueled vehicles, evaporative emissions are estimated for the refueling-spillage process only. As no results describing the speciation of spilled diesel fuel, we developed toxic fractions of total VOC based on a diesel “headspace” profile. In which the headspace is the empty space above the liquid fuel in a tank. The profile used was no. 4547 from the SPECIATE database.⁴⁹ The fractions are shown in Table 55.

Table 55. Toxic Fractions for the fuel-spillage Process, for Diesel fuel.

Pollutant	Toxic fraction
2,2,4-Trimethylpentane	0.00974
Ethyl Benzene	0.00324
N-Hexane	0.01076
Toluene	0.01419
Xylene	0.01222
Benzene	0.00410

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Appendix A: Development of Motor Vehicle Emission Factors for Mercury

Calculation of Mercury Emission Factors from Vehicle Tests

In 2005, the USEPA National Exposure Research Laboratory (NERL) collected mercury samples in the raw exhaust from 14 light-duty gasoline vehicles and two heavy-duty diesel vehicles. The work plan for this project includes details of the methods used that are not reproduced here including quality assurance and quality control for Hg collection and analysis. This information can be obtained from EPA upon request. Briefly, mercury and regulated pollutant data were collected during two sets of three consecutive LA92 drive cycles for each vehicle. The morning set of LA92 cycles began with one 'cold start' and the afternoon set of three LA92 cycles began with a 'hot start'. The intake air was filtered through charcoal to greatly reduce background mercury concentrations entering the vehicle intake. Separate sample lines were used for gaseous and particulate mercury species. Samples analyzed for mercury were drawn from raw exhaust at a constant flow rate and fixed dilution. Carbon dioxide measurements were also taken in the exhaust stream where mercury samples were collected.

Mercury samples were collected in raw exhaust since previous data suggested that mercury levels might be sufficiently low to challenge mercury detection limits. This sampling method imposed a challenge in calculating emission factors since it assumes that the exhaust flow rate from the vehicle is constant. Calculation of exhaust flow and its application to the development of mercury emission rates is described below.

Evaporative losses of mercury from motor vehicles and loss of mercury during refueling were not measured. The emission of mercury through evaporative processes is expected to be negligible compared with that expected from exhaust emissions.

A description of the vehicles tested for which data were used in developing emission rates is provided in Table 1. The data collected from these vehicles in diluted exhaust in the constant volume sampler (CVS) included total hydrocarbon (THC), carbon dioxide (CO₂), nitrogen oxides (NO_x), methane (CH₄), and carbon monoxide (CO). In raw, undiluted exhaust, data collected included elemental and total gas-phase mercury, particulate mercury and CO₂. Gas-phase mercury was also measured in the intake air. Total air flow was measured for all sampling systems and corrected to standard temperature and pressure conditions. The data streams had different reporting frequencies, all due to the nature of the instrumentation. The dilute measurement of the standard emission gases (THC, CO₂, NO_x, CH₄, and CO), CVS flows, and vehicle speed were reported at 1 Hertz. The gas-phase mercury samples were analyzed at 2.5 minute intervals and particle-phase mercury samples were collected cumulatively for the duration of three consecutive LA92 cycles. Gas-phase elemental mercury in the engine intake air was measured at five-minute intervals.

Table 1. Vehicles tested for Mercury Emissions

Model Year	Make	Model	Fuel Type	Odometer (mi)	Cylinders	Displacement (L)
2005	MERCURY	GRAND MARQUIS LS	Gasoline	9,953	8	4.6
2005	FORD	MUSTANG CONVERTIBLE	Gasoline	5,424	6	4.0
2003	SATURN	L 200	Gasoline	29,667	4	2.2
2002	HONDA	ACCORD EX	Gasoline	51,824	4	2.3
2001	HONDA	ACCORD EX	Gasoline	88,611	4	2.3
2001	CHRYSLER	PT CRUISER	Gasoline	54,010	4	2.4
2000	CHEVROLET	SUBURBAN	Gasoline	39,787	8	6.0
2000	JEEP	CHEROKEE SPORT	Gasoline	48,468	6	4.0
1999	FORD	F250 XLT	Diesel	113,897	8	7.3
1999	FORD	F250 XLT SD	Diesel	109,429	8	7.3
1998	HONDA	CIVIC DX	Gasoline	204,983	4	1.6
1994	CHEVROLET	SILVERADO	Gasoline	129,521	8	5.7
1992	CHEVROLET	S10 BLAZER	Gasoline	162,249	6	4.3
1991	HONDA	ACCORD EX	Gasoline	143,289	4	2.2
1987	CHRYSLER	FIFTH AVENUE	Gasoline	72,573	8	5.2
1984	FORD	F150 PICKUP	Gasoline	36,727	8	5.8

Exhaust flow was integrated at the same reporting frequency as the mercury exhaust values for a particular test and then used to calculate total, elemental, and reactive gas-phase mercury mass emissions. The intake air mercury values were typically collected at half the frequency of the mercury exhaust values. There is precedent in accepting background values measurements at less frequent intervals and using them to correct exhaust measured values that are reported at higher frequencies. The particulate matter measurements were filter-based, test-level measurements and were reported in that manner.

Calculation of Emission Rates

The time-series for the regulated pollutants and mercury were aligned; however, emissions data were not related to vehicle specific power as the data are not to be used estimate modal emissions modeling. Emission rates were calculated separately for elemental gas-phase mercury, reactive gas-phase mercury and particulate mercury. Elemental gas-phase mercury in the exhaust was corrected for the intake air concentration of elemental mercury. To estimate the gas-phase mercury concentration in dilute exhaust from the measured mercury in raw exhaust, the dilution factor was applied. For light-duty gasoline vehicles, the dilution factor equation found in 40 CFR 90.426 (d) was used:

$$\text{Dilution factor} = 13.4 / ([\text{CO}_2\%] + ([\text{THC, ppm}] + [\text{CO, ppm}]) * 0.0001)$$

$$\text{Exhaust flow} = (\text{CVS flow} / \text{dilution factor})$$

Exhaust flow calculation was initiated when the analytical equipment indicated that the dilute exhaust CO₂ concentration was greater than the background CO₂ concentration.

To calculate exhaust flow for the diesel vehicles, the dilution factor was calculated by simply dividing CO₂ in the raw exhaust by CO₂ in the CVS. This method was used because diesel engines operate across a very wide range of fuel to air mixtures and the CFR method described above was not appropriate.

Determination of Reactive Gas Mercury Mass in Exhaust

Reactive gas-phase mercury (RGM) was calculated by subtracting elemental gas-phase mercury measurements from total gas-phase mercury measurements. RGM values were typically small and therefore influenced by the variability in the elemental mercury measurements. Negative RGM values for a given measurement period were observed. Values for which there was not a positive RGM measurement were treated as non-detects and were nulled in the aggregation of RGM values for the test. The measurement uncertainty for gas-phase elemental mercury was estimated from quantitative recovery of injections of known amounts of mercury into the sampling system. The uncertainty in measuring elemental mercury was applied to the total gas-phase and elemental gas-phase measurements to determine when the RGM value was above the measurement uncertainty. Values within the measurement uncertainty were not included in the emission factor calculation.

Calculating Weighted Emission Test Results

Highway vehicle tests on the LA92 cycle, a more aggressive chassis-dynamometer test similar in concept to the Federal Test Procedure's (FTP) UDDS or LA4. Like the FTP, the LA92 includes a cold start, a hot start, and a hot stabilized phase using identical drive schedules for the starts. It was, therefore, considered appropriate to follow the precedent of calculating a weighted emission factor (representing cold start and hot start driving) for each vehicle in the same manner as the FTP, using the equation below for each test (a test consisting of all six LA92 cycles performed on each vehicle).

We summed the gas-phase mercury mass emissions for the first phase (300 seconds) of the morning test and last phase (1,135 seconds) of the individual LA92 drive schedules for all the tests (e.g., 'hot stabilized emissions'), divided by the total distance covered in these phases and multiplied by 0.43. We also summed the sum of the mass gas-phase mercury emissions of the first phase of the afternoon test and last phase (1,135 seconds) of all the tests, divided by the total distance covered in these phases and multiplied by 0.57. The two terms were summed to calculate a test level emission rate for each of the gasoline powered vehicles.

Equation used to calculate test-level emission rates:

$$\bar{E}_{\text{Hg}} = 0.43 \left(\frac{C + R}{C_m + R_m} \right) + 0.57 \left(\frac{H + R}{H_m + R_m} \right)$$

Where:

E_{Hg} = mean aggregate emission rate (g/mi),

C = mercury mass collected in the first 300 seconds of the first morning test ('cold start', g),

C_m = distance covered in the cold start phase (mi),

R = mercury mass collected in the last 1,135 seconds of all six cycles of the LA92 ('hot stabilized', g)

R_m = cumulative distance covered in all six cycles of the LA92 ('hot stabilized', mi)

H = mercury mass collected in the first 300 seconds of the first afternoon test ('hot start', g)

H_m = distance covered by the hot start (mi)

It should be noted that the 'hot start' in the afternoon typically occurred after the vehicle had been off for at least 1 hour, making this start closer to a 'cold start' than 'hot start'. Since the true cold start emissions were slightly higher than hot start emissions, it is expected that this approach would bias the emission factors high by a small amount, relative to the value expected for a cycle composite.

Particulate mercury emissions could not be apportioned into modes of operation in similar manner because filters were collected across all three LA92 cycles and could not be parsed into the three phases. A test-level emission rate was calculated by multiplying the morning particulate mercury emission rate by 0.43 and the afternoon particulate mercury emission rate by 0.57 and adding the two values together.

The average of emission factors across vehicles was calculated for each form of mercury and is reported in Table 2. A simple average was used since the data did not suggest that mercury concentrations varied by vehicle age, mileage, displacement or other factors.

Mercury emission factors for on-road diesel engines were obtained from the first 715 seconds of the morning and afternoon tests on the Ford F250 XLT SD; data from the second diesel vehicle could not be used. The first 715 seconds is approximately half of the first of the three LA92 drive cycles that made up a single test. The truncation of the test was due to sample flow problems in the mercury sampling manifold due to particulate matter restricting flow across the particulate matter filters. Graphical analysis of exhaust flow indicated that they appeared nominal during the first LA92 cycle. It was decided that only using data collected before 715 seconds into both tests provided the most reliable data.

Table 2. Mercury Emission Factors from Mobile Sources

Source Category	Pollutant	Pollutant ID	Emission Rate	Units
Gasoline motor vehicles	Elemental gas-phase	200	1.1E-07	grams/mile
	Reactive gas-phase	201	9.9E-09	grams/mile
	Particulate phase	202	4.0E-10	grams/mile
Diesel motor vehicles	Elemental gas-phase	200	6.2E-09	grams/mile
	Reactive gas-phase	201	3.2E-09	grams/mile
	Particulate phase	202	1.6E-09	grams/mile
Gasoline nonroad engines	Elemental gas-phase	200	1.8E-06	grams/gallon
	Reactive gas-phase	201	1.7E-07	grams/gallon
	Particulate phase	202	6.9E-09	grams/gallon
Diesel nonroad engines	Elemental gas-phase	200	1.2E-07	grams/gallon
	Reactive gas-phase	201	6.2E-08	grams/gallon
	Particulate mercury	202	3.2E-08	grams/gallon