1	Macro- and Micro-Purge Soil Gas Sampling Methods
2	for the Collection of Contaminant Vapors
3	
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6	
7	Abstract
8	Purging influence on soil gas concentrations for volatile organic compounds (VOCs), as
9	affected by sampling tube inner diameter and sampling depth (i.e., system volume) for temporary
10	probes in fine-grained soils, was evaluated at 3 different field sites. A macro-purge sampling
11	system consisted of a standard hollow 3.2 cm outer diameter (OD) drive probe with a retractable
12	sampling point attached to an appropriate length of 0.48 cm inner diameter (ID) Teflon® tubing.
13	The macro-purge sampling system had a purge system volume of 24.5 mL at a 1 m depth. In
14	contrast, the micro-purge sampling systems were slightly different between the field sites and
15	consisted of a 1.27 cm OD drive rod with a 0.10 cm ID stainless steel tube or a 3.2 cm OD drive
16	rod with a 0.0254 cm inner diameter stainless steel tubing resulting in purge system volumes of
17	1.2 mL and 7.05 mL at 1 m depths, respectively. At each site and location within the site, with a
18	few exceptions, the same contaminants were identified in the same relative order of abundances
19	indicating the sampling of the same general soil atmosphere. However, marked differences in
20	VOC concentrations were identified between the sampling systems with micro-purge samples
21	having up to 27 times greater concentrations than their corresponding macro-purge samples. The
22	higher concentrations are the result of a minimal disturbance of the ambient soil atmosphere
23	during purging. The minimal soil gas atmospheric disturbance of the micro-purge sampling

1 system allowed for the collection of a sample that is more representative of the soil atmosphere 2 surrounding the sampling point. That is, a sample that is not does not contain an atmosphere that 3 has migrated from distance through the geologic material or from the surface in response to the 4 vacuum induced during purging soil gas concentrations. It is, thus, recommended that when soil 5 gas sampling is conducted using temporary probes in fine-grained soils, that the sampling system 6 uses the smallest practical ID soil gas tubing and minimize purge volume to obtain the soil gas 7 sample with minimal risk of leakage so that proper decisions, based on more representative soil 8 gas concentrations, about the site can be made.

9

10 Introduction

11 Soil gas data are widely used in site investigation and remediation projects to delineate 12 volatile organic compound (VOC) vapor plumes, as a screening tool to refine soil and 13 groundwater sampling efforts, to track the progress of soil remediation, and to identify potential 14 risks from the inhalation of indoor air associated with soil vapor migration and intrusion into 15 buildings and homes (EPA 2007). The overall goal of any monitoring or sampling program is to 16 collect representative samples; that is, samples that are representative of the environmental, chemical, and physical conditions present during the time of sample collection. However, due to 17 18 numerous environmental, as well as sampling and analytical variables, the representativeness of 19 a sample can often be compromised, the degree to which is often not well understood or 20 quantified. The definition of a representative sample is also dependent upon the data quality 21 objectives of the sampling effort. In some cases, a larger sample and corresponding larger 22 sampling area is desired to account for heterogeneity in the subsurface. In other cases, a discrete

sample that best characterizes the VOC concentrations at that sampling point and depth is
 desired.

3 A number of research groups and local, state, and federal agencies have developed 4 guidance concerning sampling and analytical protocols for active soil vapor sampling with the 5 overall objective of facilitating a technically correct approach for site investigations (EPA 2007). 6 Guidance documents from a variety of sources including the: American Petroleum Institute (API 7 2005); American Society for Testing and Materials (ASTM 2001); California Environmental 8 Protection Agency, Department of Toxic Substances Control and California Regional Water 9 Quality Control Board, Los Angeles Region (CaEPA 2003); Interstate Technology and 10 Regulatory Council (ITRC 2007); Missouri Department of Natural Resources (MoDNR 2005); 11 New Jersey Department of Environmental Protection (NJDEP 2005); New York State 12 Department of Health (NYSDH 2005); and the U.S. Environmental Protection Agency (EPA 13 2006), all generally recommend that purge volume be minimized to increase the likelihood that 14 the collected sample is representative of conditions immediately surrounding the sampling probe 15 and to reduce the potential of short-circuiting (i.e., the intrusion of surface air into the sample via 16 channeling down the probe tube) the sampling system. However, few of the documents provide 17 specific recommendations for purge volumes. CaEPA (2003) guidance stipulates that a step 18 purge test be conducted by collecting samples after one, three, and seven line volumes have been 19 purged. MoDNR (2005) and NJDEP (2005) recommend three line volumes be purged prior to 20 sampling while NYSDH (2005) recommends one to three line volumes.

The system volume refers to the total volume of gas purged prior to sample collection
(EPA 2007). Most soil vapor sampling protocols require the purging of a system volume
consisting of multiple line volumes prior to collection of the final sample for analysis. However,

1 during purging, the ambient soil atmosphere in the immediate vicinity of the probe tip, which is 2 in theoretical equilibrium with the all soil fractions (e.g., air, water, mineral and organic matter), 3 is removed. The resultant soil gas collected for analysis migrated from the geologic material 4 immediately surrounding the probe tip in response to the vacuum induced during purging, unless 5 the geologic material has a lower permeability than the annulus between the probe and the 6 geologic materials, in which case, there may be short circuiting with soil gas flowing from the 7 next shallower higher permeability geologic interval. There may also be complexities in 8 fractured media or where soil macropores act as a preferential flow pathway, if purge volumes 9 are very large.

10 Soil gas sampling protocols also recognize that large system volumes in sampling trains 11 require correspondingly large purge volumes (EPA 2007). As the purge volumes increase, 12 associated with larger sampling tube diameters and deeper sampling depths, more and more of 13 the ambient soil atmosphere is lost prior to sample collection and the size of the recharge zone 14 increases. The resultant analytical samples may represent the "average" conditions within the 15 larger purged area; however, the area of influence is not known. In areas with very little 16 localized vapor phase VOCs or relatively tight soils (i.e., high clay content soils) using 17 temporary probes, there is a greater chance of short-circuiting to shallower more permeable 18 intervals, such that an analytical false negative can result. Conversely, limiting system volume 19 purging requirements increases the likelihood that the sample is representative of a discrete, 20 limited volume immediately adjacent to the sampling location that is representative of the 21 ambient VOC concentrations found at the location prior to purging. This paper describes the 22 influence of system volume removal during purging, as affected by sampling tube diameters and

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1	sampling depth, on the concentrations of VOCs found at several contaminated waste sites with
2	silt and clay-rich soils using temporary driven probes.

4 Materials and Methods

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6 Sampling Locations

Three sites contaminated with volatile organic compounds were selected to test the
macro- and micro-purge soil gas sampling systems. These sites were located at Mare Island
Naval Shipyard (MINS) in Vallejo, CA; Grants Chlorinated Solvents Plume (GCSP) in Grants,
NM; and Vandenberg Air Force Base (VAFB) Installation Restoration Project Area 3, near
Lompoc, CA. At each site, multiple locations were sampled. The distance between each pair of
macro- and micro-purge system sampling points was approximately 30 cm.

13

14 **Probe Design**

15 The design of the macro-purge sampling system remained the same at all three sites while 16 the design of the micro-purge sampling system was the same at the MINS and GCSP sites and 17 altered, to allow for greater depth of sampling, at the VAFB site. Although not specifically 18 designed for use in fine-grained soils, the Post-Run Tubing (PRT) system by Geoprobe® 19 (Geoprobe, 2003) was used for the macro-purge soil-vapor sampling system. A hollow 3.2 cm 20 OD drive probe with a retractable sampling point was inserted to the appropriate depth (1m 21 below ground surface [bgs] at MINS and GCSP and between 2.4 and 3.7 m bgs at VAFB). The 22 drive probes were then raised approximately 2.5 - 5.0 cm to create a void in the subsurface. A 23 section of FEP Teflon[®] tubing (0.49 cm ID x 0.64 cm OD) was attached to a threaded PRT

adapter, inserted down the hollow probe tube and threaded into the retractable probe tip housing.
The other end of the Teflon® tubing was attached to a septum port constructed from a 0.6 cm
Swagelok® elbow fitting through which a syringe was inserted to collect a sample. The internal
volume of the macro-system at 1m bgs was calculated as 18.1 mL for the tubing, plus 6.4 mL to
account for the internal volume of the retractable drive-point, for a total internal volume of 24.5
mL.

7 To collect the micro-purge vapor samples at the MINS and GCSP sites, the soil-vapor 8 sampling system designed by Hewitt (1998) was used (Figure 1). The probe design consisted of 9 a small-diameter stainless steel tubing (0.16 cm OD and 0.10 cm ID) epoxied into a grove in a 10 1.2 m steel drive rod. The upper end of the stainless steel tubing extending out the top of the 11 probe and was attached to a Swagelok[®] septum port. On the bottom end of the probe, a 12 disposable, conical, brass drive point was fitted onto the end of the sampling tube to assist in 13 probe placement and to prevent soil from clogging the stainless steel tubing. After the probe was 14 driven to a 1 m depth, the probe was raised approximately 2.5 cm to create a void in the 15 subsurface. The internal volume of the sampler was approximately 1.2 mL at a 1m sampling 16 depth.

To allow for sampling at greater depths, such as found at the VAFB site, a variation of the Hewitt micro-volume system was necessary. The modified probe design (Figure 2) consisted of a small-diameter stainless steel tubing (0.0254 cm ID) epoxied into a Geoprobe[®] PRT point holder such that the open end of the steel tubing (Sigma Aldrich[®] part number 20552) was approximately 2.8 cm below mouth of the point holder (i.e., the depth necessary for the insertion of the expendable drive point). For sampling, the stainless steel tubing was run through the hollow shaft of the probe rod during insertion and then capped with a low dead volume

Swagelok[®] union with Teflon[®] lined septa. After the probe was driven to the appropriate depth,
 the probe was raised approximately 2.5 cm to create a void in the subsurface. The internal
 volume of the sampler was approximately 7.05 mL at 1m bgs, 0.05 mL for the stainless steel
 tubing and 7.0 mL the internal volume of the expendable point holder.

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6 Sample Collection

At each site, soil vapor samples were collected after purging 3 system volumes. A gastight glass syringe with on/off valve (SGE 8970 for 10 mL and SGE 9770 for 100 mL) was used to collect a volume equal to one purge system volume for analysis. To collect the samples, the syringe plungers were to drawn back at a rate to minimize the creation of a vacuum. At the VAFB site, after soil vapor samples were collected, the on/off valve was closed, the end of the syringe needle capped via insertion into a septa, and taken directly to an on-site mobile laboratory for analysis.

14 At the MINS and GCSP sites, the collected gas samples were transferred to thermal 15 desorption tubes (TD) tubes (Pankow et al. 1998). The TD tubes were stainless steel, 8.9 cm long by 0.64 cm diameter, sealed at each end with brass Swagelok[®] endcaps fitted with Teflon[®] 16 17 ferrules. Each TD tube contained 180 mg Carbotrap B on the inlet side, followed by 70 mg 18 Carboxen 1000 (Supelco Inc., Bellefonte, PA). During sampling, the end caps were removed 19 and an on/off valve, with a septum port, was attached to the front end of the TD tube and a 20 constant flow air sampling pump (Sensidyne, Clearwater, FL) on the tail end. The pump 21 maintained a constant flow of 50 mL/min of filtered ambient air through the TD tube. To 22 transfer the sample, with the pump running, the valve was opened and the sample injected near 23 the front of the TD tube. The air flow through the tube was maintained for a minimum of 15 min

before the valve was closed. The TD tubes were capped and stored chilled (4° C) prior to
 analysis.

Bulk soil samples were collected at the MINS and GCSP sites using a 60 mm diameter core sampler (Geoprobe[®] RS60) driven to the appropriate depth. The core tube was then brought to the surface and an 8 cm segment, containing the sampling depth, was collected for the determination of particle-size distribution and total organic carbon content (TOC).

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8 Sample Analysis

Soil vapor samples were analyzed using a modified version of EPA Method TO-17 (EPA
1997a) and quantified using the gas chromatography/mass spectrometry technique described in
SW-846 Method 8260B (EPA 1997b) at the MINS and GCSP sites. At the VAFB site, soil
vapor samples were analyzed by direct injection using EPA SW-846 method 8021B (EPA 1996).
Soil particle-size analyses were determined using the hydrometer method as specified in
Gee and Bauder (1986). TOC determinations were performed following the high-temperature
induction furnace method of Nelson and Sommers (1996).

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17 Quality Assurance/Quality Control

Quality assurance/quality control (QA/QC) measures included trip and field blanks; spiked samples; field duplicate samples (sequential collection of a second system volume after purging); and initial and ongoing calibration checks. All field and laboratory quality control sample results were compliant with the project specific data quality objectives. Leak testing was performed at the VAFB site using a rag saturated with 1,1-difluoroethane (DFA), placed over the surface completion of the probe. No DFA was detected in any of the samples associated with the leak checks indicating no short circuiting to the surface although cross communication between
 different depth intervals below the surface could still be possible.

3

4 **Results and Discussions**

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6 Mare Island Naval Shipyard

7 The soil at the MINS site had a silt loam texture and a TOC of 1.5% (Table 1). VOCs 8 identified at the MINS site included toluene, ethylbenzene, and xylenes (Table 2 and Figure 3). 9 At both locations, the relative order of abundance of the contaminants was the same between the 10 micro-purge and macro-purge systems. When the contaminants were identified in both the 11 micro-purge and macro-purge systems, at location 1, the concentrations were about 5 times 12 greater in the micro-purge samples than the macro-purge samples while at location 2, the 13 concentrations were between 15 and 22 times greater in the micro-purge samples than the macro-14 purge samples.

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16 Grants Chlorinated Solvent Plume

The soil at the GCSP site had a silt loam texture and a TOC of 0.4% (Table 1). VOCs identified at the GCSP site included tetrachloroethene (PCE), trichloroethene (TCE), *cis*-1,2dichloroethene (DCE), toluene, ethylbenzene, and xylenes (Table 2 and Figure 3). PCE was the dominant contaminant and had a concentration of 27.8 μ g/L when collected using the micropurge system and 3.1 μ g/L when collected using the macro-purge system. When the contaminants were identified in both micro-purge and macro-purge samples, concentrations were markedly higher in the micro-purge samples. The concentration differences ranged from the same for o-xylene to 23 times higher for m, p-xylenes in the micro-purge samples than the macro-purge samples. All contaminants found in the macro-purge samples were identified in the micro-purge samples. Conversely, toluene was not indentified in the macro-purge samples yet was identified in the micro-purge samples. Possible explanations for the lack of toluene in the macro-purge samples include analytical loss/error or loss during purging combined with the subsequent lack of recharge from the surrounding soil.

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8 Vandenberg Air Force Base

9 The soil at the VAFB site had a clayey sand texture (G. Swanson, personal 10 communication, July 21, 2008). The primary contaminant identified at all three locations on 11 VAFB was TCE. DCE was found only at locations 2 and 3. TCE concentrations ranged from 12 270 to 1500 μ g/L in the micro-purge samples (Table 2) and from 26 to 120 μ g/L in the macro-13 purge samples. When identified, the concentrations of DCE were low relative to the 14 concentrations of TCE. At location 2, DCE was found at 2.5 and 1.3 μ g/L in the micro-purge 15 and macro-purge samples, respectively. Similarly, at location 3, the concentrations of DCE 16 found in the micro-purge and macro-purge samples were 12 and 2.6 μ g/L, respectively. The 17 TCE concentrations were 9 to 27 times greater in the micro-purge samples than the macro-purge 18 samples system (Figure 3). When DCE was identified, the micro-purge sample contained about 19 2 to 5 times as much as the macro-purge sample.

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21 Conclusions

At each of the sites and each location within the sites, although there were variations in texture and total organic carbon contents, the same contaminants (with few exceptions) were

1 identified using either the micro-purge or macro-purge temporary probe systems. In general, the 2 relative abundances of the identified contaminants were identical until VOC concentrations 3 approached the detection limits. When the relative abundances orders were different between the 4 two sampling systems, it was generally the case where the contaminant was identified with the 5 micro-purge sampling system and not detected with the macro-purge sampling system. These 6 results indicate that the same soil atmosphere was being collected by both sampling systems. 7 However, when a larger purge volume was required, the larger purge volumes may have led to 8 the loss of any detectable levels of toluene as these contaminants were identified only when 9 using the micro-purge sampling system at the GCSP site. Macro-purge sample volumes were 10 about 20 times greater at the MINS and GCSP sites and 6 to 10 times greater at the VAFB site 11 than the micro-probe sample volumes collected at the same depths.

12 The concept that the larger purge volumes required when using a macro-purge sampling 13 system led to a greater loss and subsequent reduction in contaminant concentrations is supported 14 by the markedly higher concentrations of each contaminant found in the micro-purge samples. 15 Concentrations ranged from the same to 27 times greater in the micro-purge samples than their 16 corresponding macro-purge samples. The higher concentrations are the result of a minimal 17 disturbance of the ambient soil atmosphere during purging or less cross-communication along 18 the outer annulus of the drive casing. The minimal disturbance allows for the collection of a 19 sample that is more representative of the soil atmosphere surrounding the sampling point and a 20 sample that does not contain an atmosphere that has migrated from distance through the geologic 21 material or from the surface in response to the vacuum induced during purging soil gas 22 concentrations. It is thus, recommended that when soil gas sampling is performed using 23 temporary probes in fine-grained soils, that the sampling system uses the smallest practical ID

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soil gas tubing and minimize the purge volume to obtain a final soil gas sample that has minimal risks of atmospheric air leakage so that proper decisions, based on more representative soil gas concentrations, about the site can be made. Otherwise, probes should be installed with sandpacks around the screened interval and bentonite slurry above the sandpack through the annulus between the probe and the borehole wall.

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Table 1. Soil Characteristics							
SITE	% Sand	% Silt	% Clay	% TOC			
\mathbf{MINS}^{\dagger}	15	78	7	1.5			
GCSP [†]	13	79	8	0.4			
Note: MINS = Mare Island Navel Shipyard, GCSP = Grants Chlorinated Solvent Plume.							
\dagger - n = 3-5 replicates per site.							

"Trichloroethylene cis-12-dichloroethene Tetrachloroethylene Ethylbenzene m,p-Xylene Sample ID Toluene o-Xylene ND 1.5 0.78 ND 5.0 ND ND MINS11 MINS2I ND ND 3.4 ND 0.70 2.4 1.1 GCSP4I 0.80 0.42 1.4 27.8 0.23 13 0.44 ND VAFB1I 270 ND ND ND ND ND VAFB2I 2.5 700 ND ND ND ND ND VAFB3I 12 1500 ND ND ND ND ND 0.44 0.15 MINS1A ND ND 0.68 ND 0.11 0.05 ND ND 0.23 ND 0.041 0.14 MINS2A ND 0.044 3.1 0.10 0.56 GCSP4A 0.44 0.44 29 ND ND ND ND ND ND VAFB1A 1.3 VAFB2A 26 ND ND ND ND ND ND 2.6 120 ND ND ND ND VAFB3A

Table 2. Sample Data for the MINS, GCSP, and VAFB sites.

4 Note: MINS = Mare Island Navel Shipyard, GCSP = Grants Chlorinated Solvent Plume, VAFB = Vandenberg Air Force Base, ND = non-detect.



Figure 1. MINS and GCSP Micro-Purge Sampling System



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Figure 3. Ratios of VOC concentrations between micro- and macro-purge sampling systems. (Note: Ratios only shown when VOC identified by both systems.)